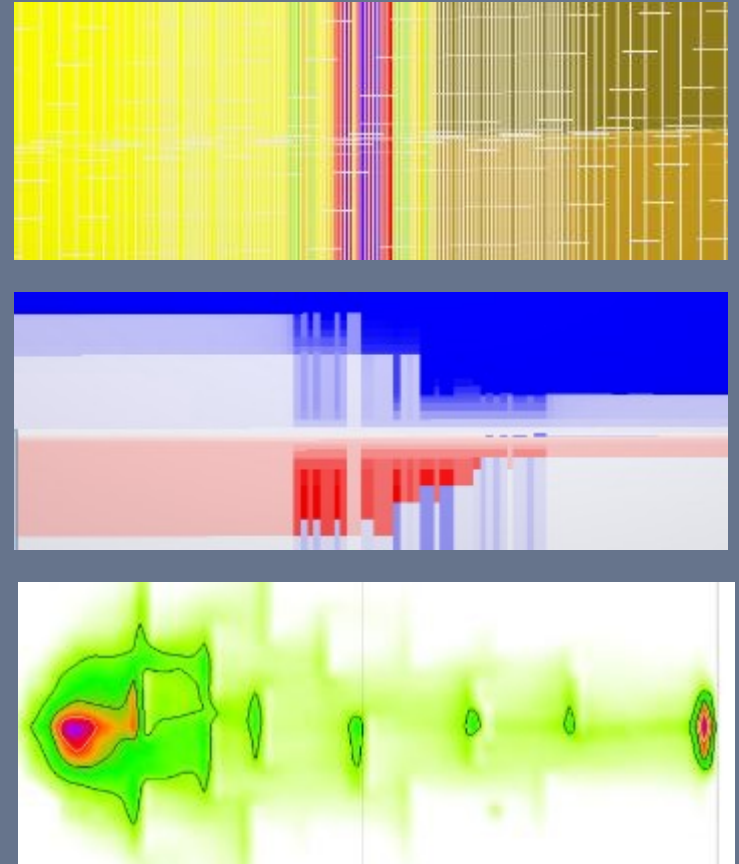


Overcoming under-forecasting

Incremental storage through cumulative residence

Mark Bentley, Ed Stephens
TRACS & Heriot-Watt University
Michael Welch, DTU

Danish CCS May 2026



One word ...

Residence

Specifically ...

*Mapping cumulative residence to
quantify the impact of structural
heterogeneity on incremental
storage calculations*



How sensitive is CCS to heterogeneity?

Critical order of magnitude perm contrasts – ‘Flora’s rule’

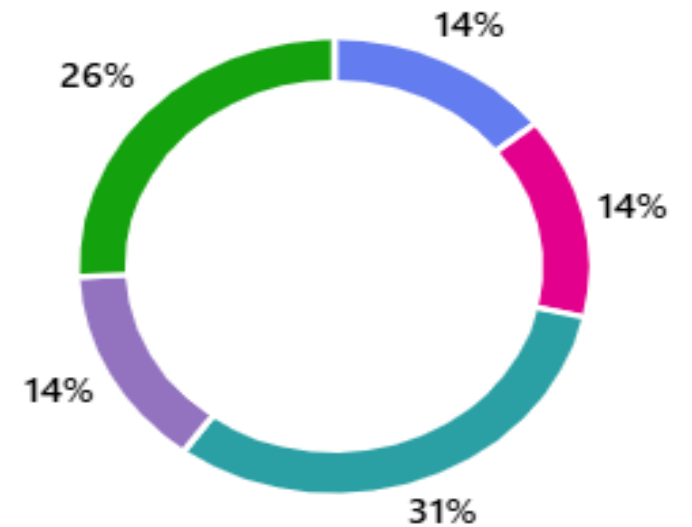
Critical permeability contrast	3 orders 2 orders 1 order			
Fluid fill	dry gas	wet gas	light oil	heavy oil
Production mechanism	depletion (no aquifer)	depletion (with aquifer)	water injection	gas/steam injection

So ... where does CCS fit on this spectrum?

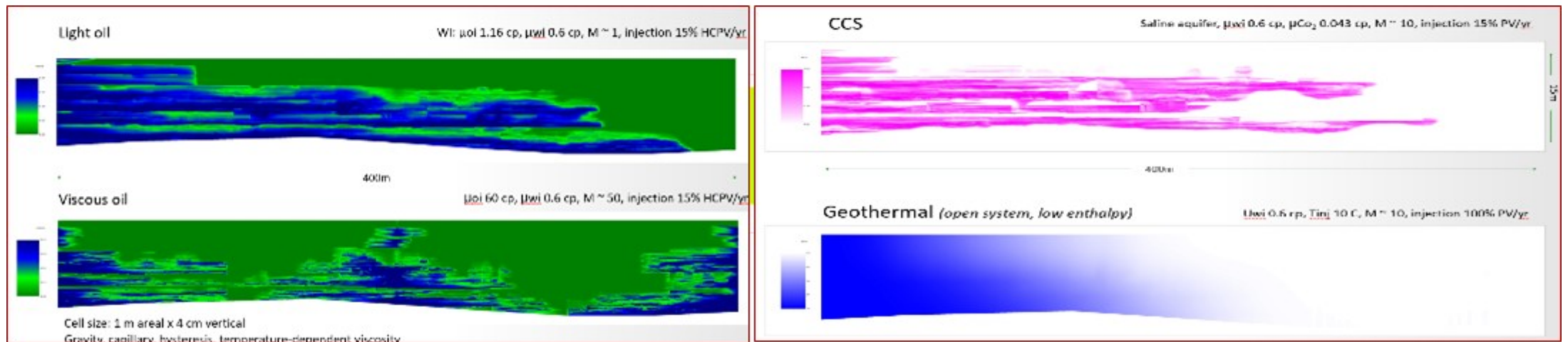
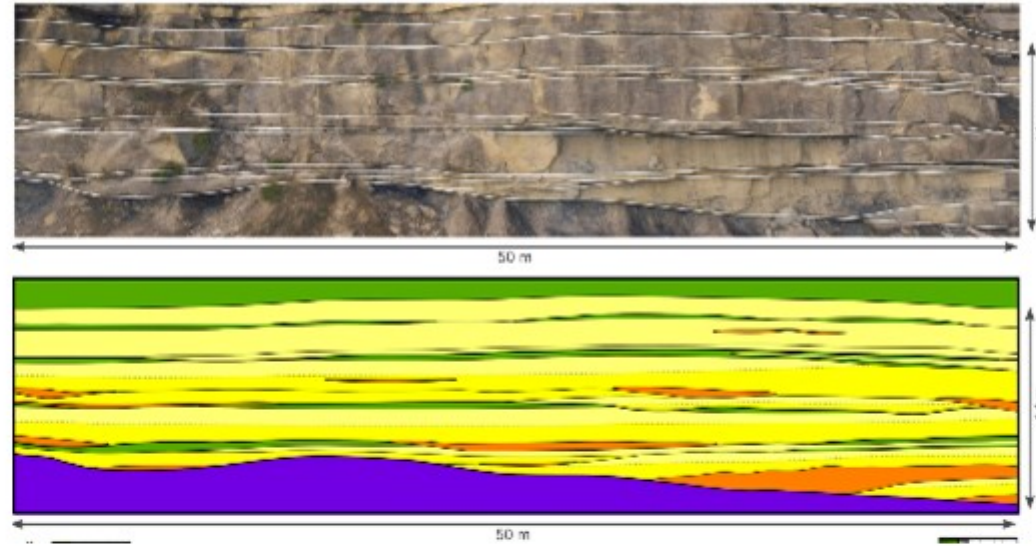
Sensitivity to permeability heterogeneity (orders of magnitude)

1. Sensitivity to permeability heterogeneity (orders of magnitude) (0 poeng)

● A - Greater than 3 orders	5
● B - 3 orders	5
● C - 2 orders	11
● D - 1 order	5
● E - Less than 1 order	9

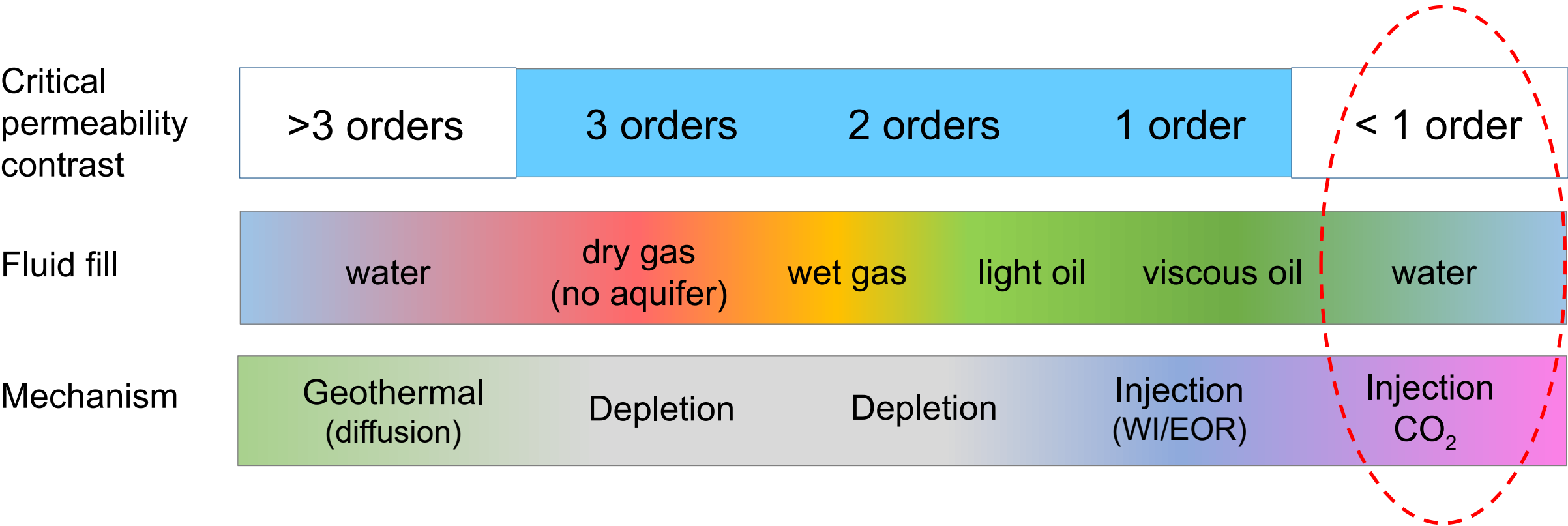


Fluid sensitivity to heterogeneity



How sensitive is CCS to reservoir heterogeneity?

Critical order of magnitude perm contrasts – “Flora plus”



Storativity & storage – what is the storage efficiency factor?

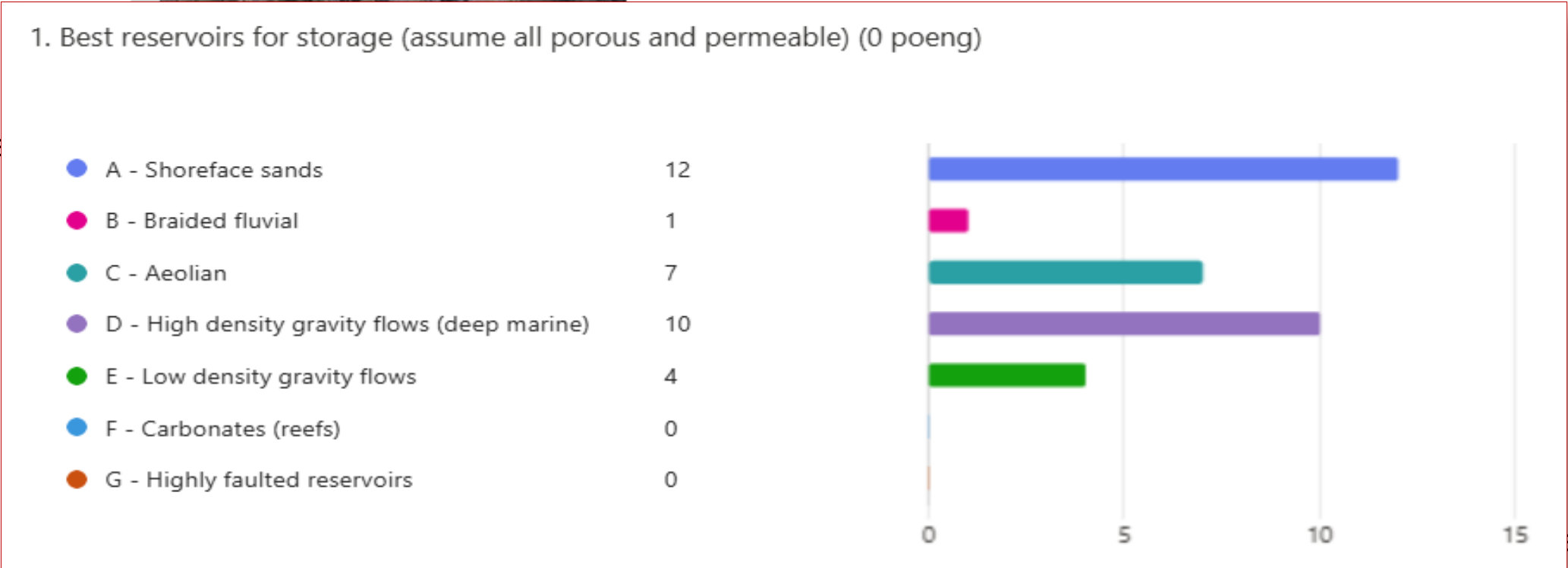
A
Middle-Upper
Shoreface



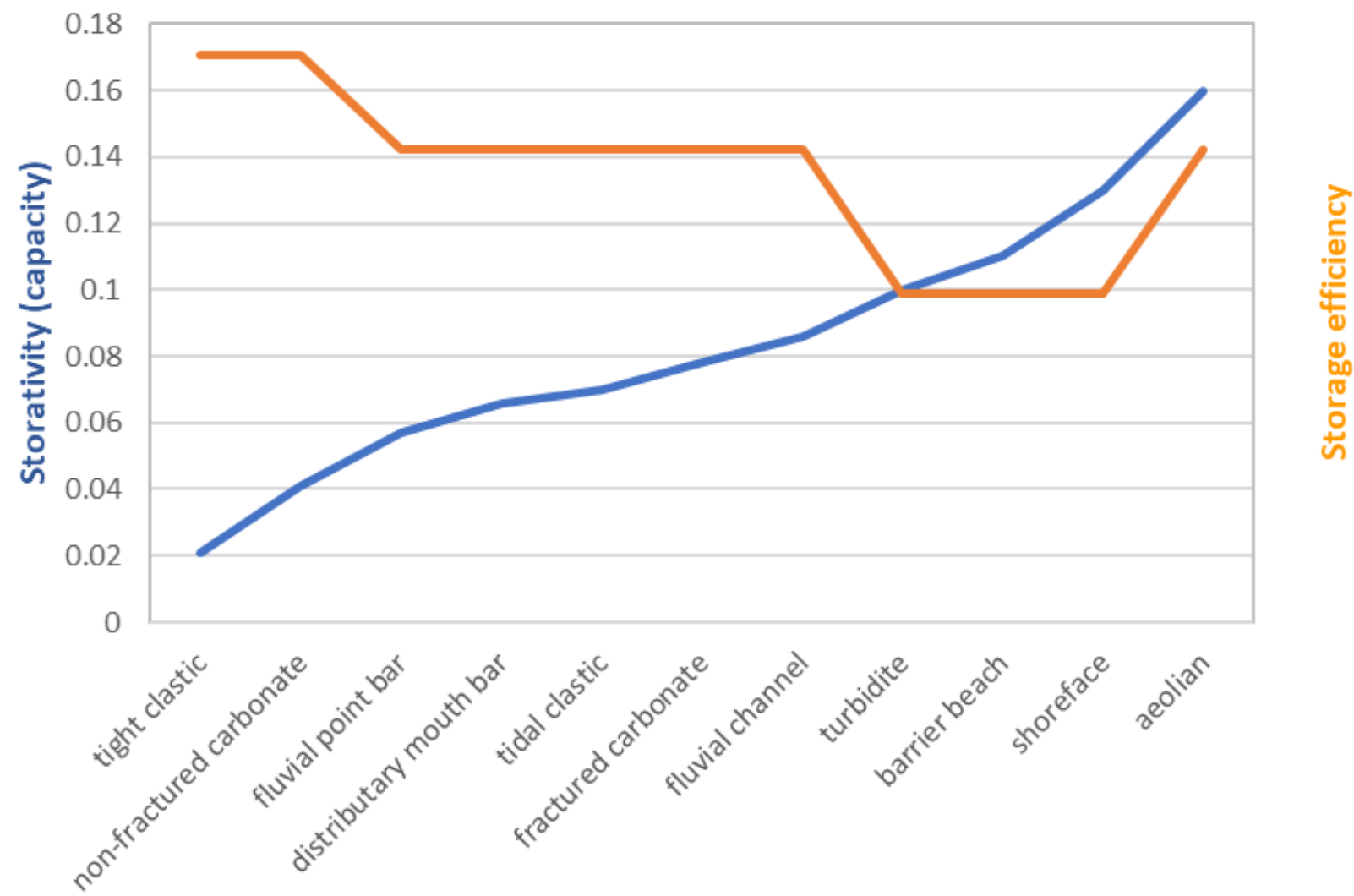
B
Fluvial channels

C
Aeolian (dune)

D
High density
gravity flow

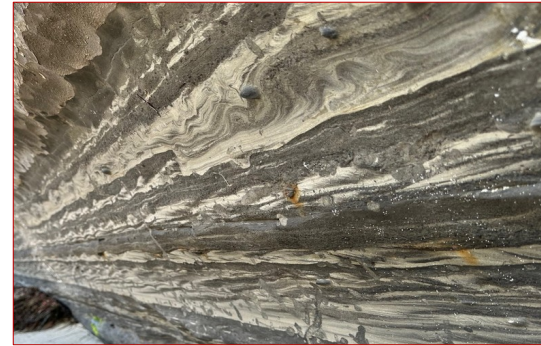
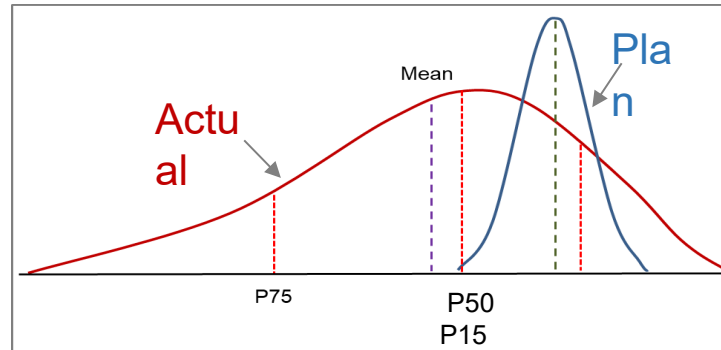


Having your cake and eating it



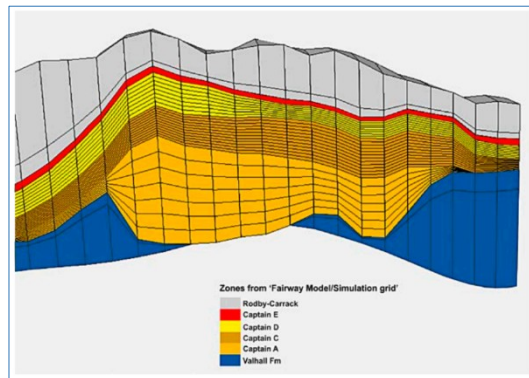
Over-forecasting and under-forecasting

Production
(including open
geothermal)



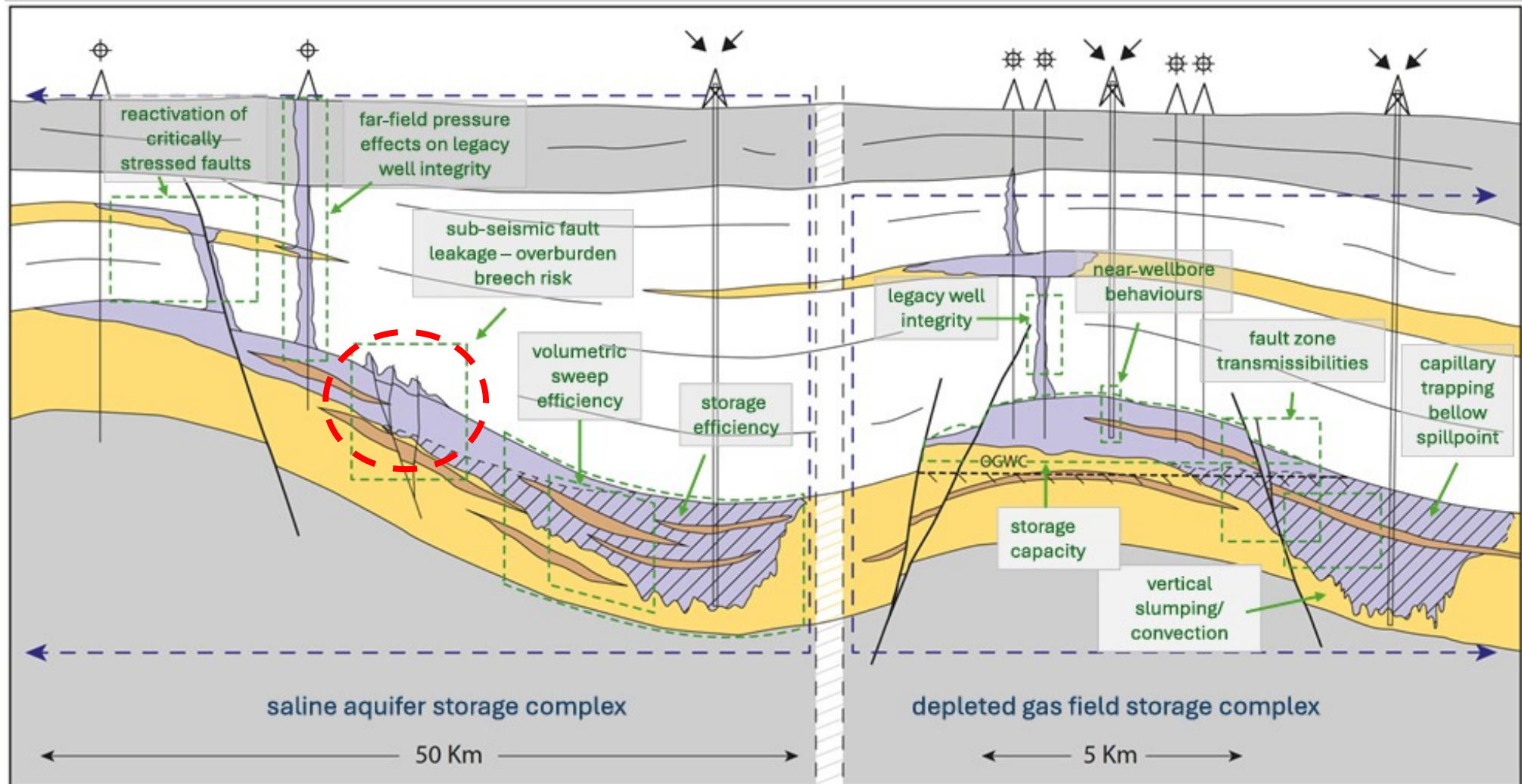
Heterogeneity
= bad news
story

Storage



Heterogeneity
= good news
story

Structural heterogeneity – sub-seismic





2D faults

... with 1D transmissibility



3D faults

*... with 3D properties
(and then REV them)*



Fault heterogeneity issues for CCS

We need to consider

The effect on the **CO2 plume**:

2 phase problem – controlled by capillary entry pressure

Faults may be completely sealing for CO2 – but it only takes one hole for the CO2 to leak

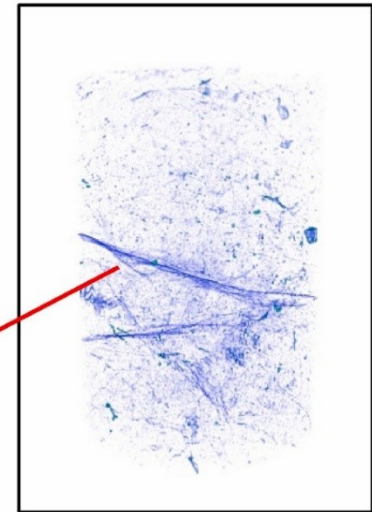
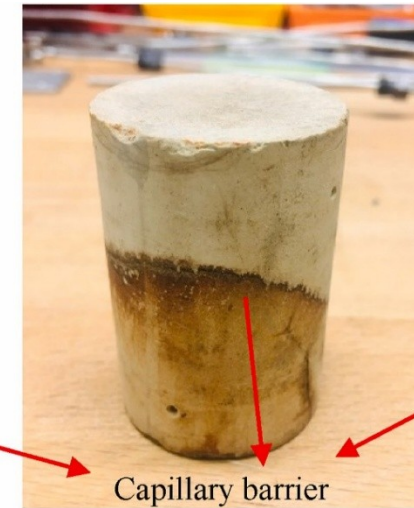
The effect on the **pressure front**:

If water can cross the fault, so can pressure

The fault may act as a baffle – water can cross, but the pressure front is slowed



*Arbuckle Mountains,
Oklahoma*



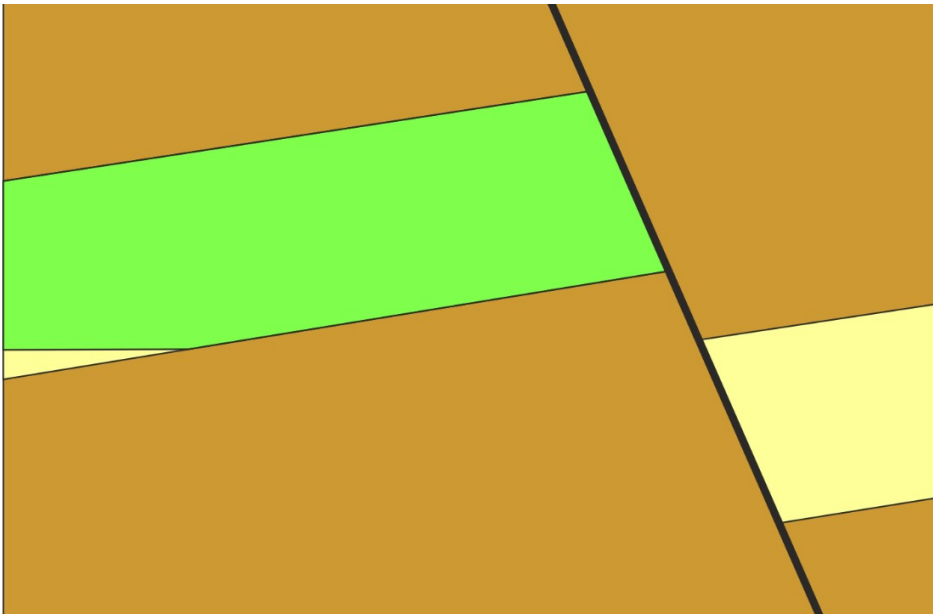
from Mokhtari et al. 2022

Fault seal types

Juxtaposition seal

The seal is reliable, as long as there are no permeable layers on the sealing side of the fault

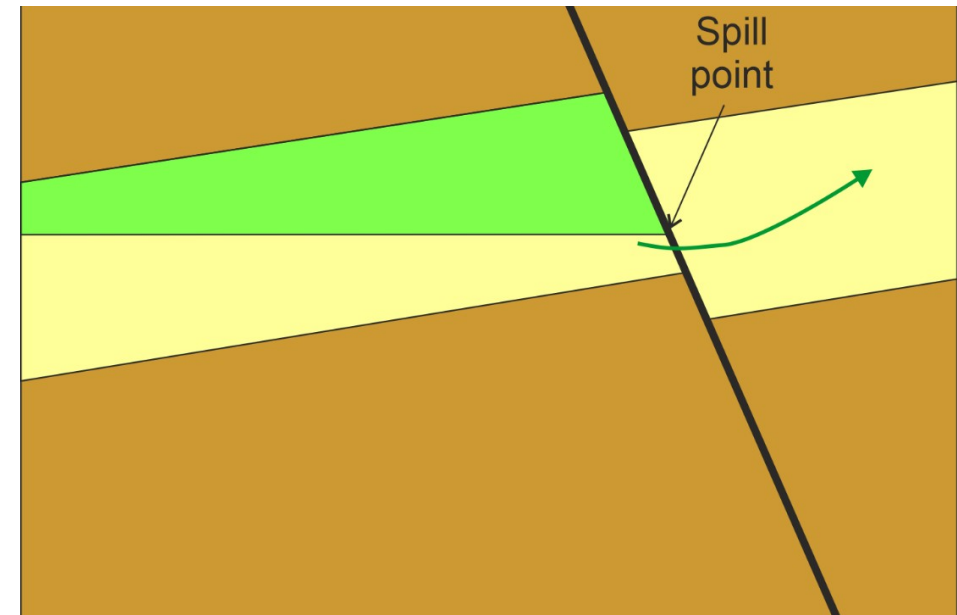
Structural trapping in the wedge



Fault rock seal

Reservoir juxtaposed so the fault itself provides the seal. Less reliable

Capillary effect

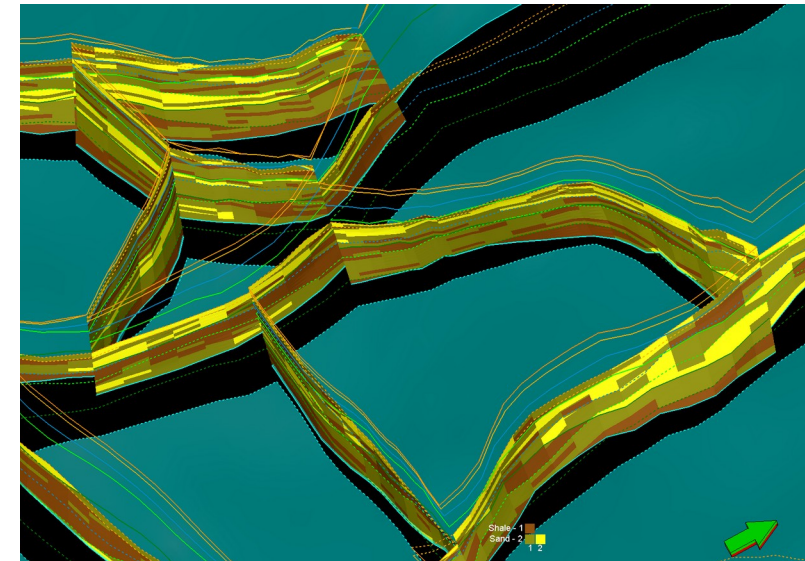


Juxtaposition seal

We can use juxtaposition diagrams to identify juxtaposition seals and leak points, and calculate wedge trapping volumes

Triangle diagrams plot stratigraphy against fault throw, to identify windows of reservoir juxtaposition. Useful when actual fault throw is not well known *e.g. sub-seismic faults*

Allan diagrams plot footwall and hanging stratigraphy along specific fault planes where the throw is known. Useful when fault geometry and throw is well constrained *e.g. seismic-scale faults*



Fault rock

What is fault rock?

A mixture of material from all layers cut by the fault, e.g. a mixture of sand and clay - **fault gouge**

Sand grains may be broken down into smaller particles by cataclasis - **grain crushing**

Fault rocks may be preferentially **cemented**

Ductile layers may remain intact, forming continuous **smears**



Northumberland, England

Fault rock

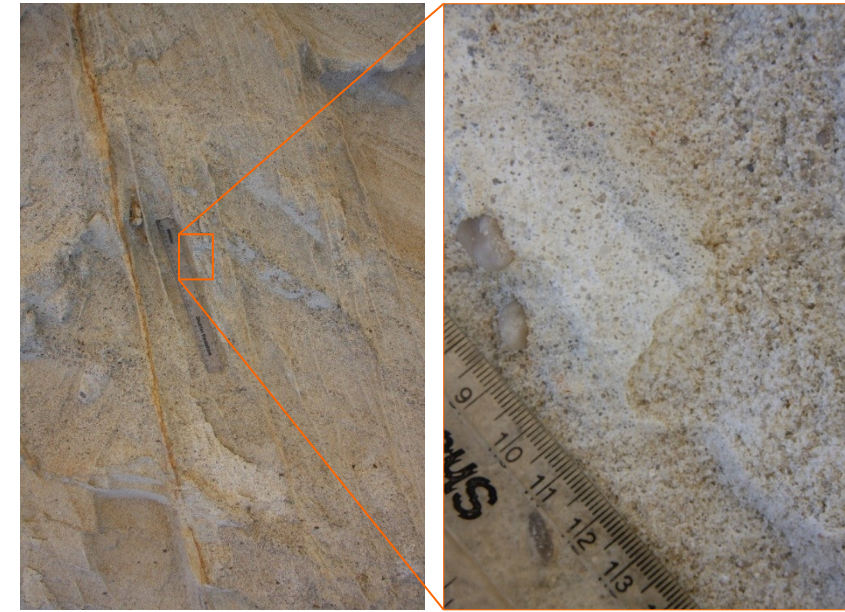
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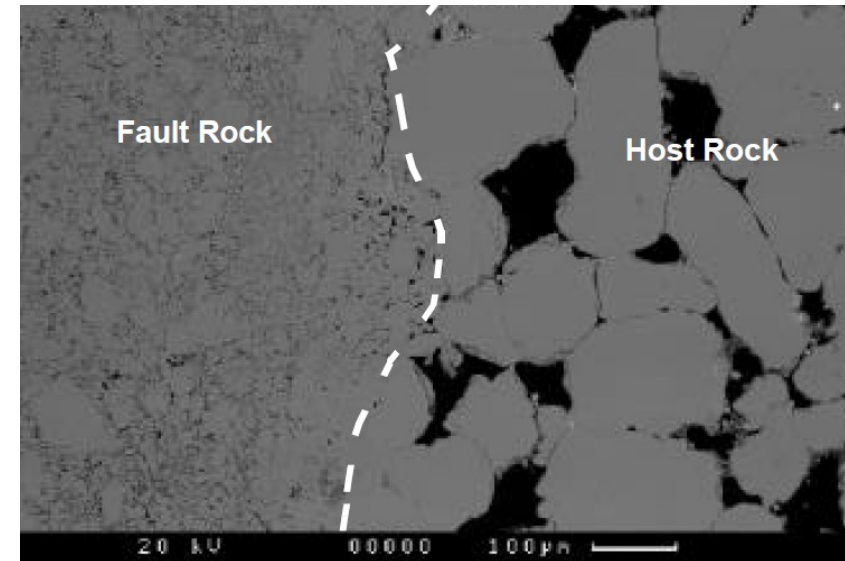
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Ductile layers may remain intact, forming continuous **smears**



Orange, France



Fault rock

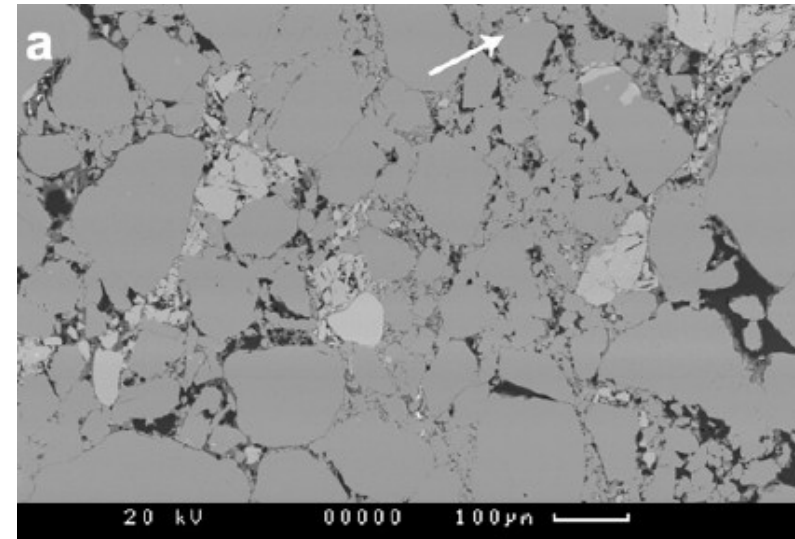
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Fault rocks may be preferentially **cemented**

Ductile layers may remain intact, forming continuous **smears**



*Quartz cementation around
cataclastic grains, from
Tueckmantel et al. 2012*

*Skull Creek,
Colorado*

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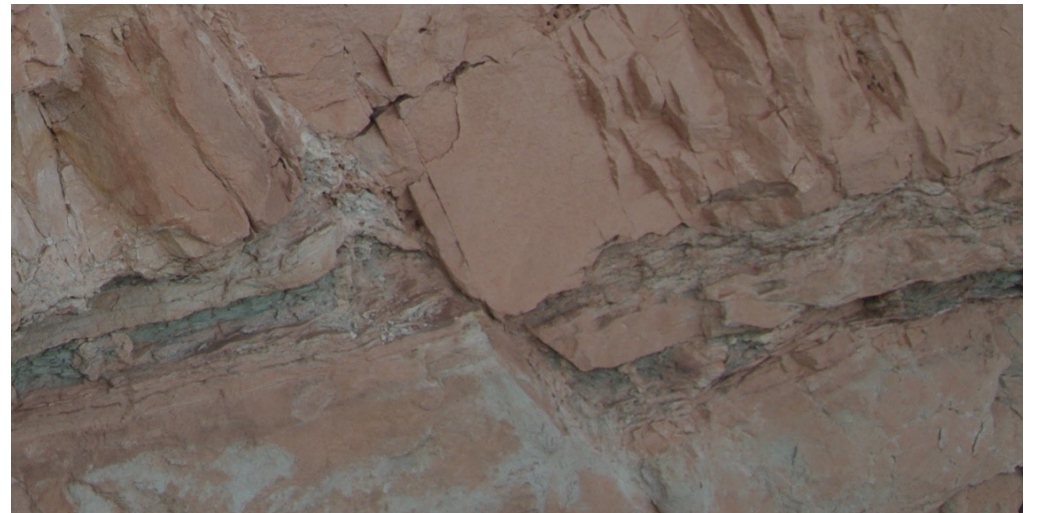
Fault rocks may be preferentially **cemented**

Ductile layers may remain intact, forming continuous **smears**

*Santa Cruz,
Portugal*



*Dinosaur,
Colorado*



Fault rock petrophysics

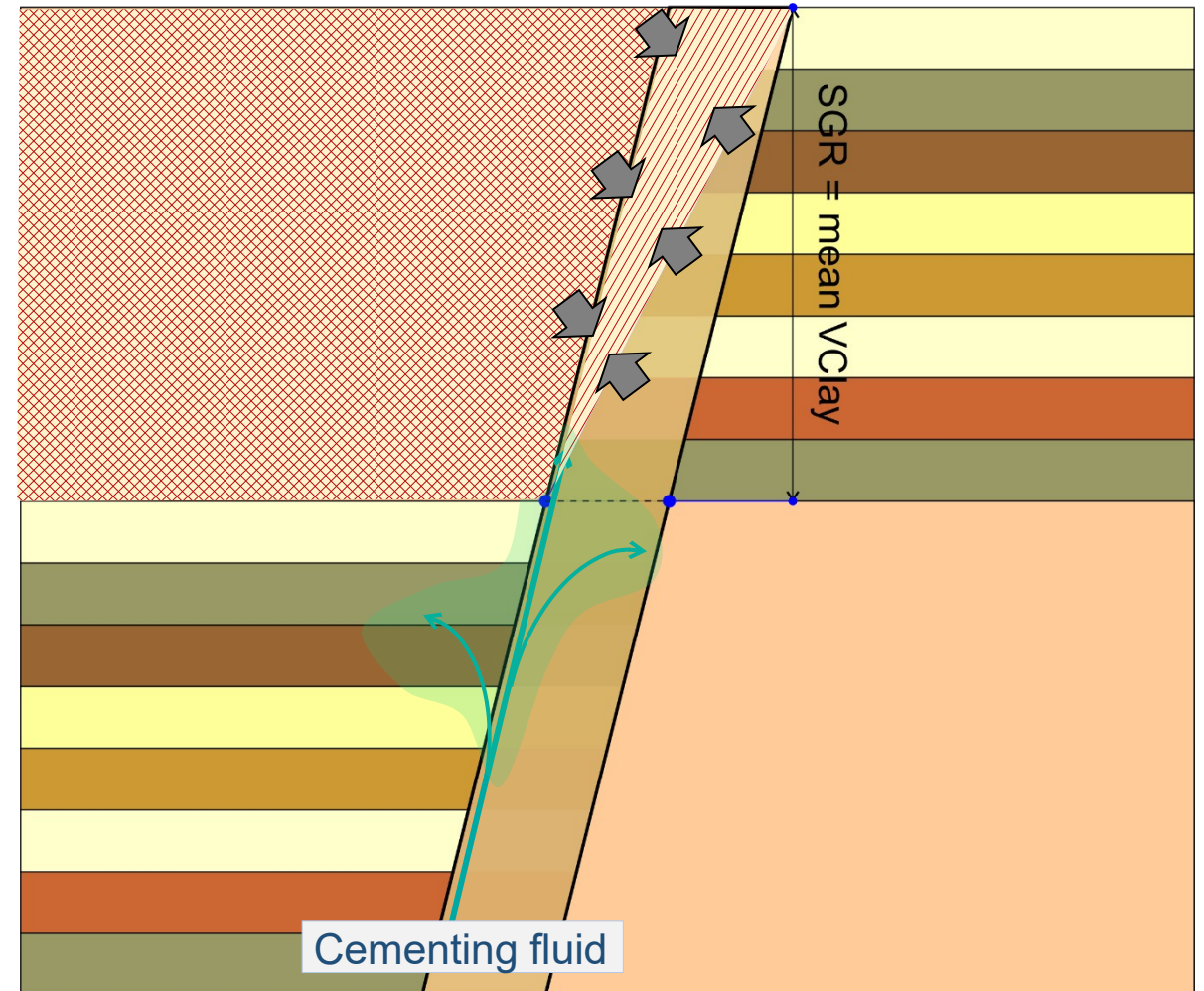
Fault rock properties are controlled by several factors

(Fisher & Knipe 1998, Fisher et al. 2003)

Fault rock **composition**, i.e. the proportion of sand and clay

Amount of **cataclasis**: the depth of burial (i.e. stress) at the time of faulting.

Amount of **cementation** - the maximum **depth of burial** after faulting (quartz cement) or fluid flow through the fault (calcite cement)



Mercury injection

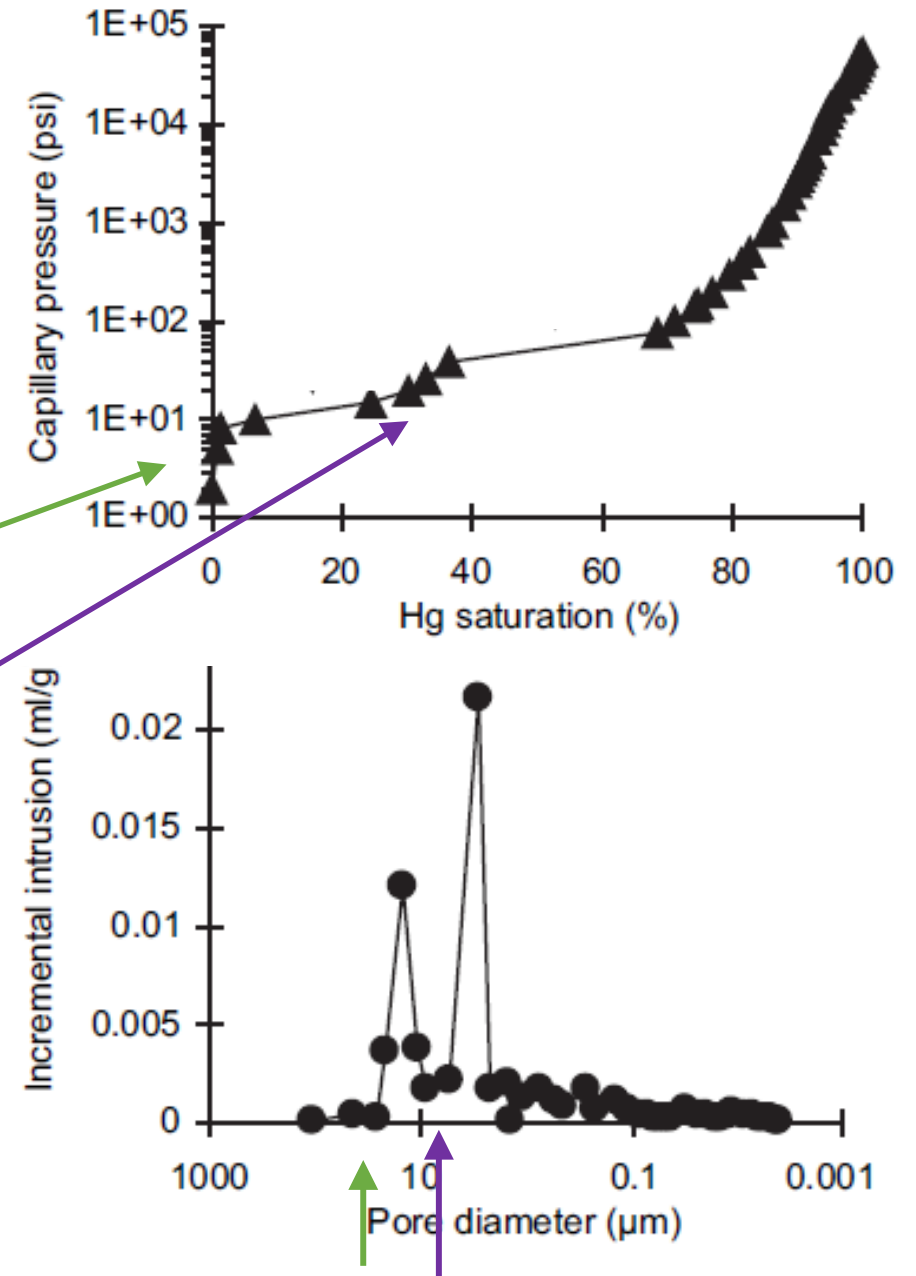
The trick is to cut the sample so the fault crosses it, and inject the mercury from one side

There will be **2 steep segments** in the injection volume / pressure curve:

The first where mercury intrudes into the first half of the sample – but is blocked by the fault; this gives the capillary entry pressure of the **host rock**

The second where mercury crosses the fault into the second half of the sample; this gives the capillary entry pressure of the **fault rock**

By measuring samples from different faults, we can cross-plot fault rock capillary entry pressure against fault rock clay content



Fault rock capillary entry pressure vs clay content

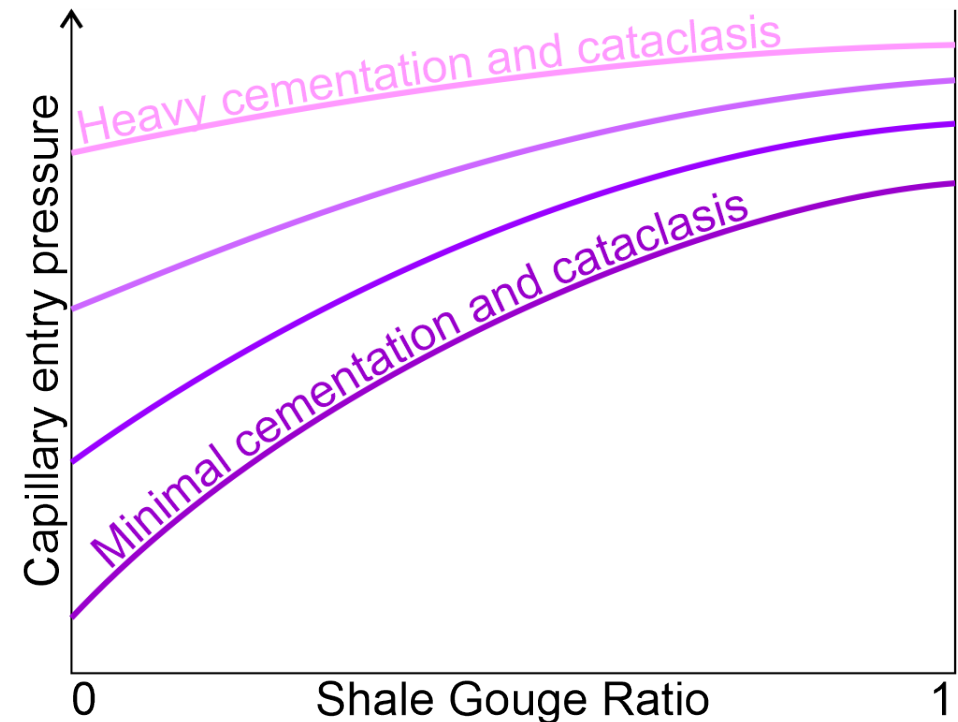
Faults with more cataclasis and/or cementation will have a low gradient and high values – generally good seals

Faults with less cataclasis and/or cementation will have a high gradient and low values – poor seals, especially at low clay content

We can then compare the curves with the calculated SGR to estimate capillary trap volume

Note that there are some generic curves published in the literature – e.g. Sperrevik et al. 2002

Care must be taken when using these as they are very generic and take no account of local conditions



Fault zone architecture

So far we have considered faults as a single flat plane

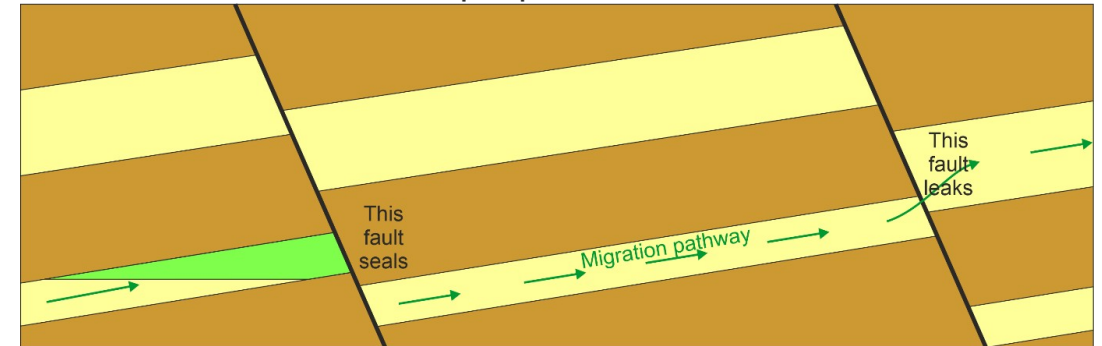
In reality faults are multi-planar objects with detailed internal architecture and geometry (see papers by Walsh et al, Knipe et al, Fossen et al, Peacock & Sanderson)

Complex fault zone architecture can provide potential leak pathways not obvious from simple fault seal analysis, e.g.:

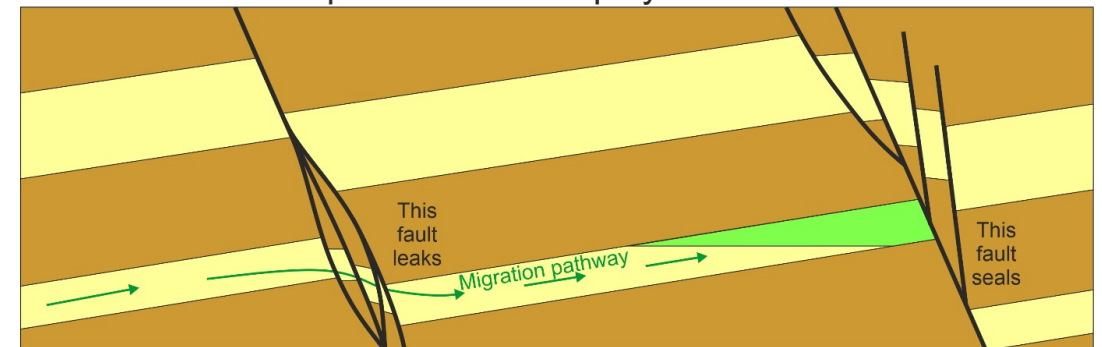
Fault bound lenses: for multiple fault strands, the throw on each strand < total throw, so seal calculations will be inaccurate - reservoir units may be juxtaposed on each strand, allowing additional flow

Relay zones: in 3D, faults tend to segment along strike; throws die out in the relay zones between segments, allowing additional flow

Simple planar faults



Complex faults with splays and lenses



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Northumberland, England

Fault zone architecture

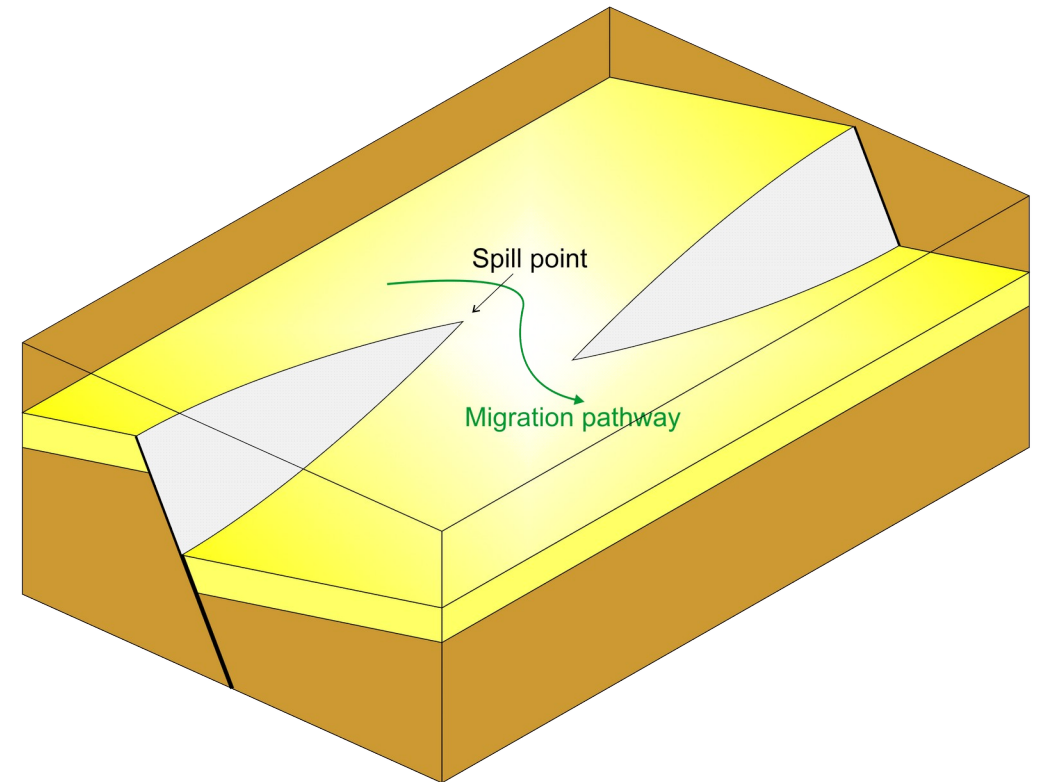
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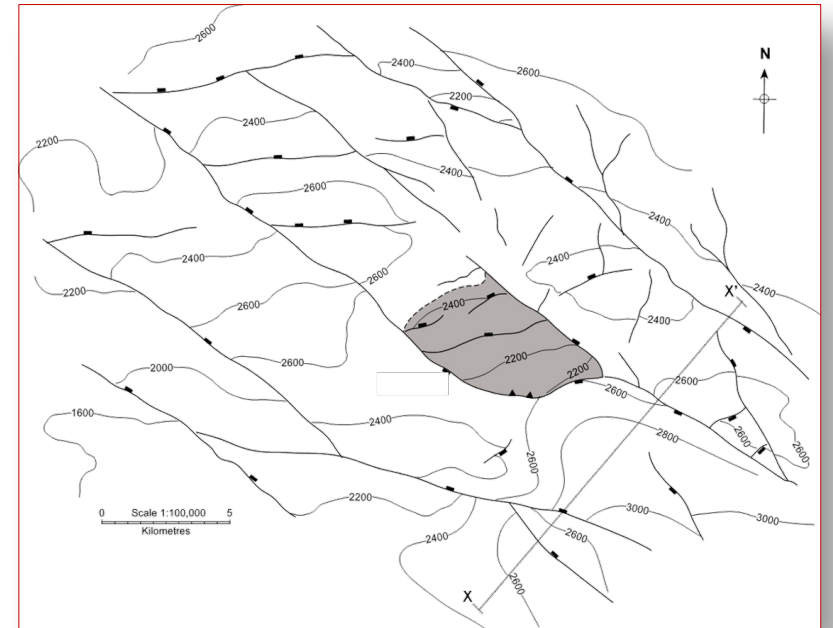
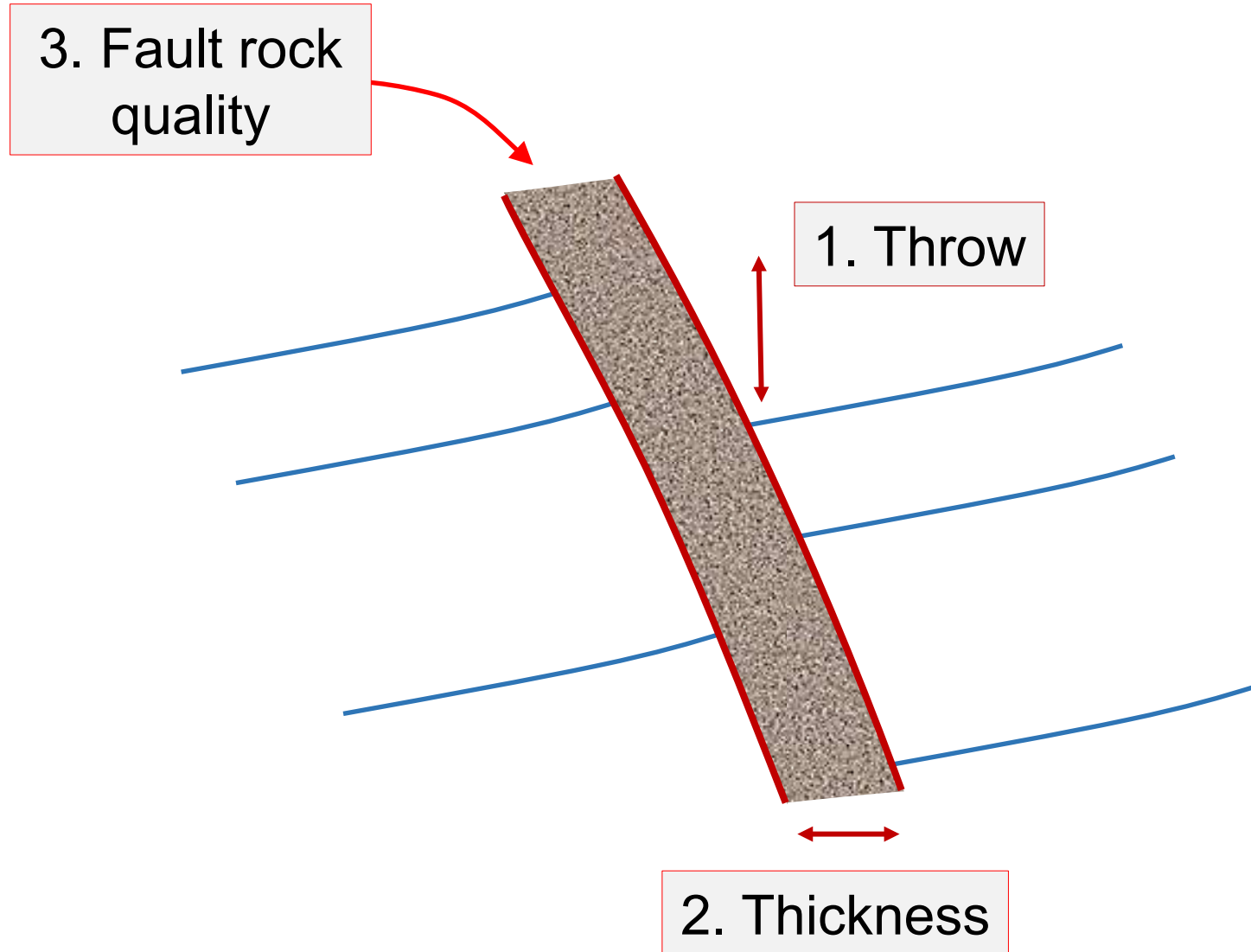
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Moab, Utah

Parameterising 'Fault Intensity'



How many faults ... ?

Fault analogues

Narrow damage zone



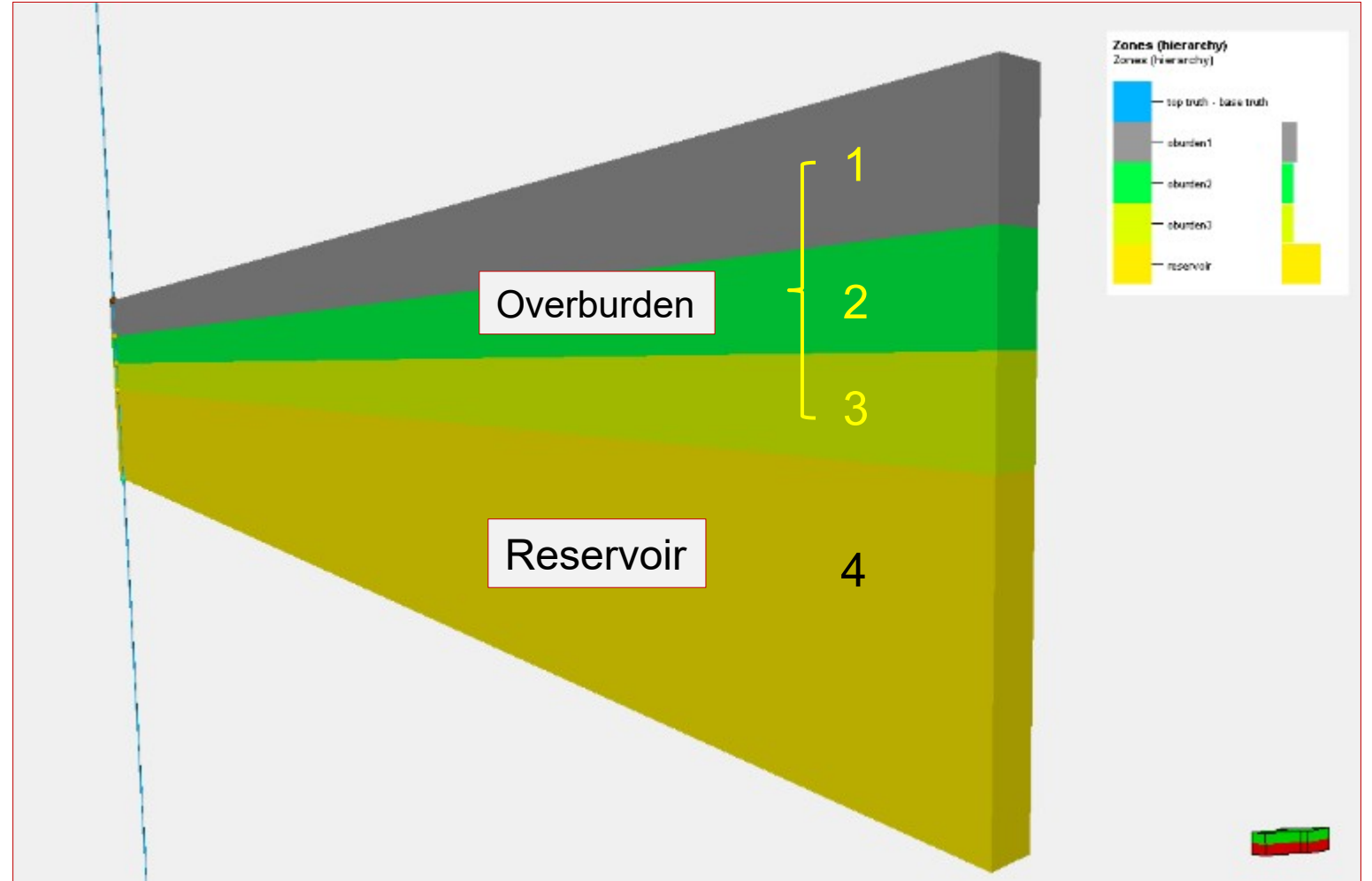
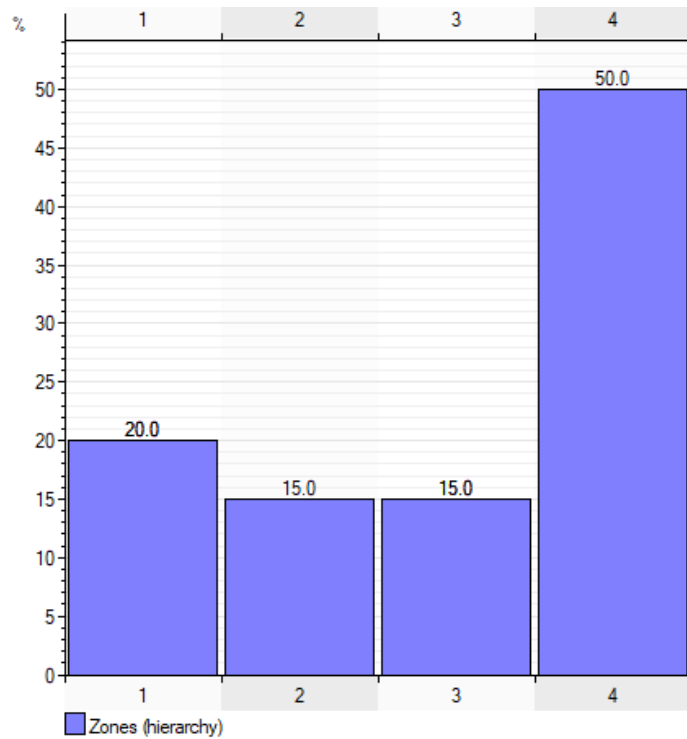
Wide damage zone



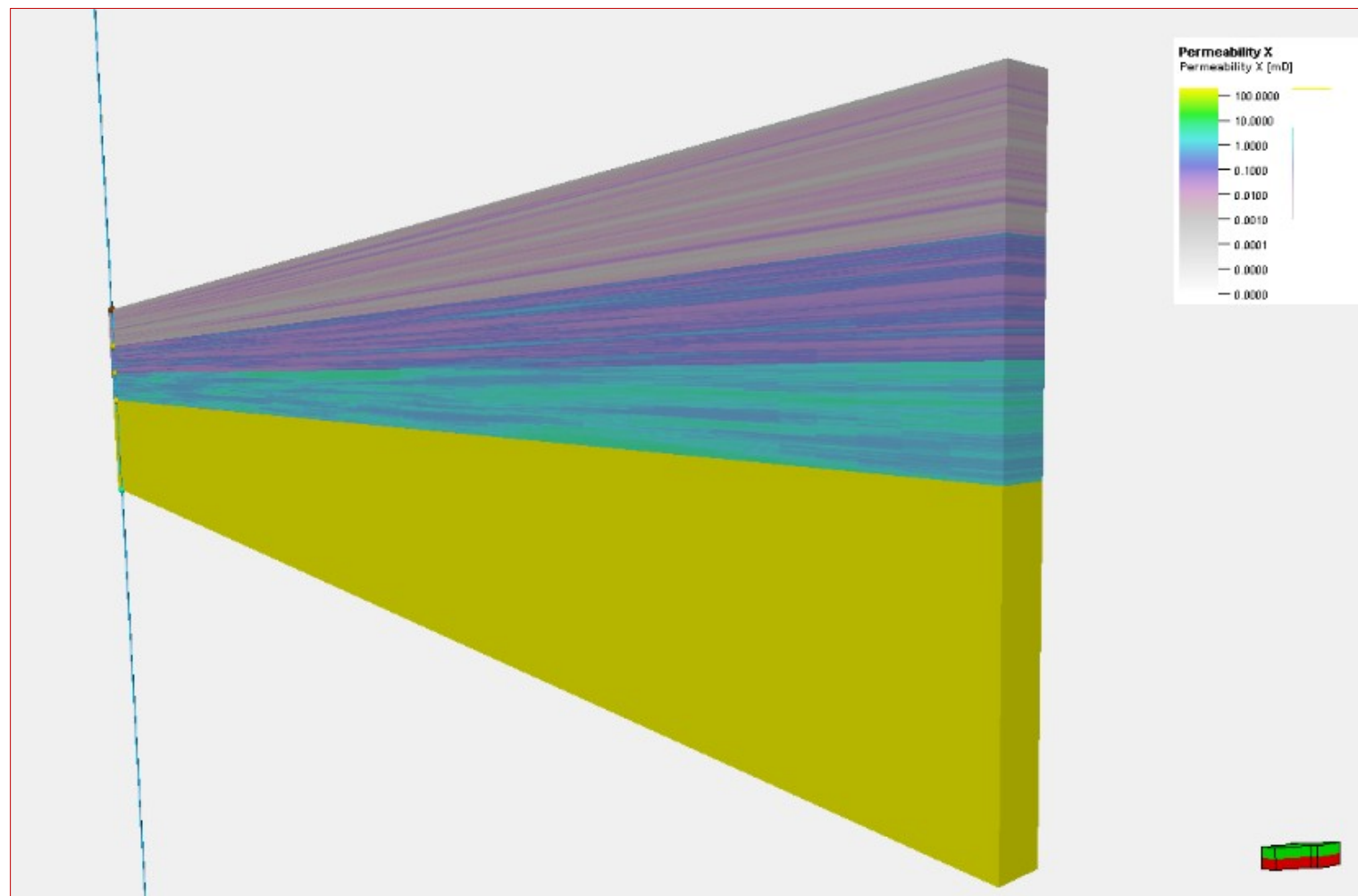
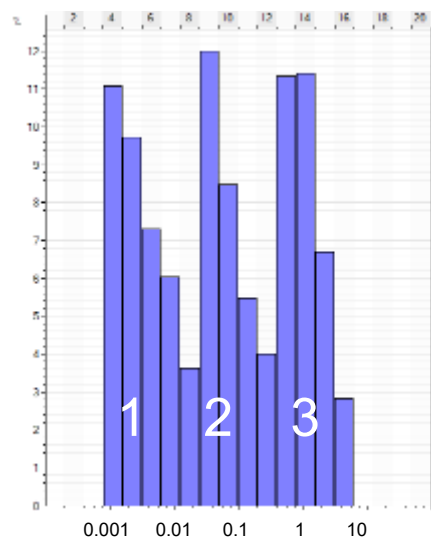
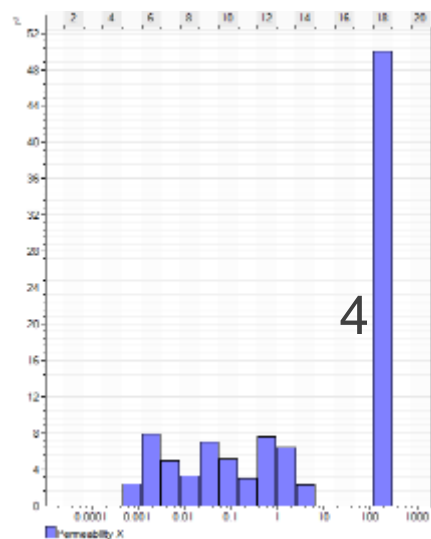
Cemented



Zones (ca. host rock types)



Permeability X



Damage zone profiles

10m throw	10m throw	10m throw	no throw	no throw
1m damage zone	1m dz with cement	50cm damage zone	50cm damage zone	10cm damage zone

Fault elements

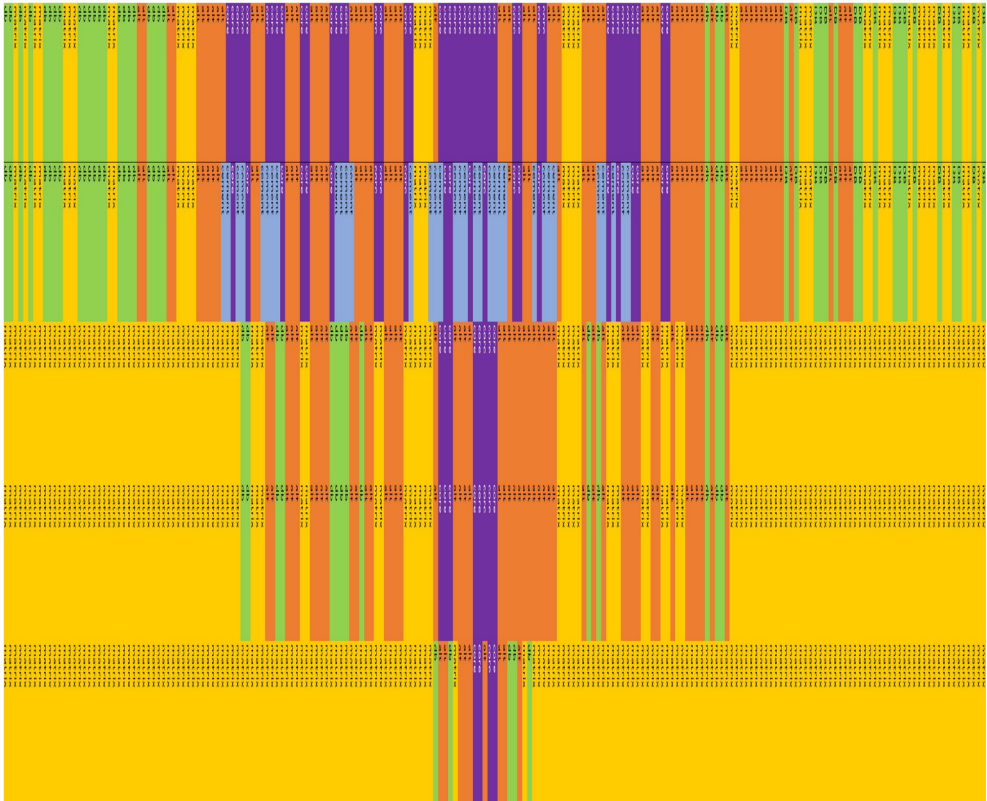
fault core

altered matrix

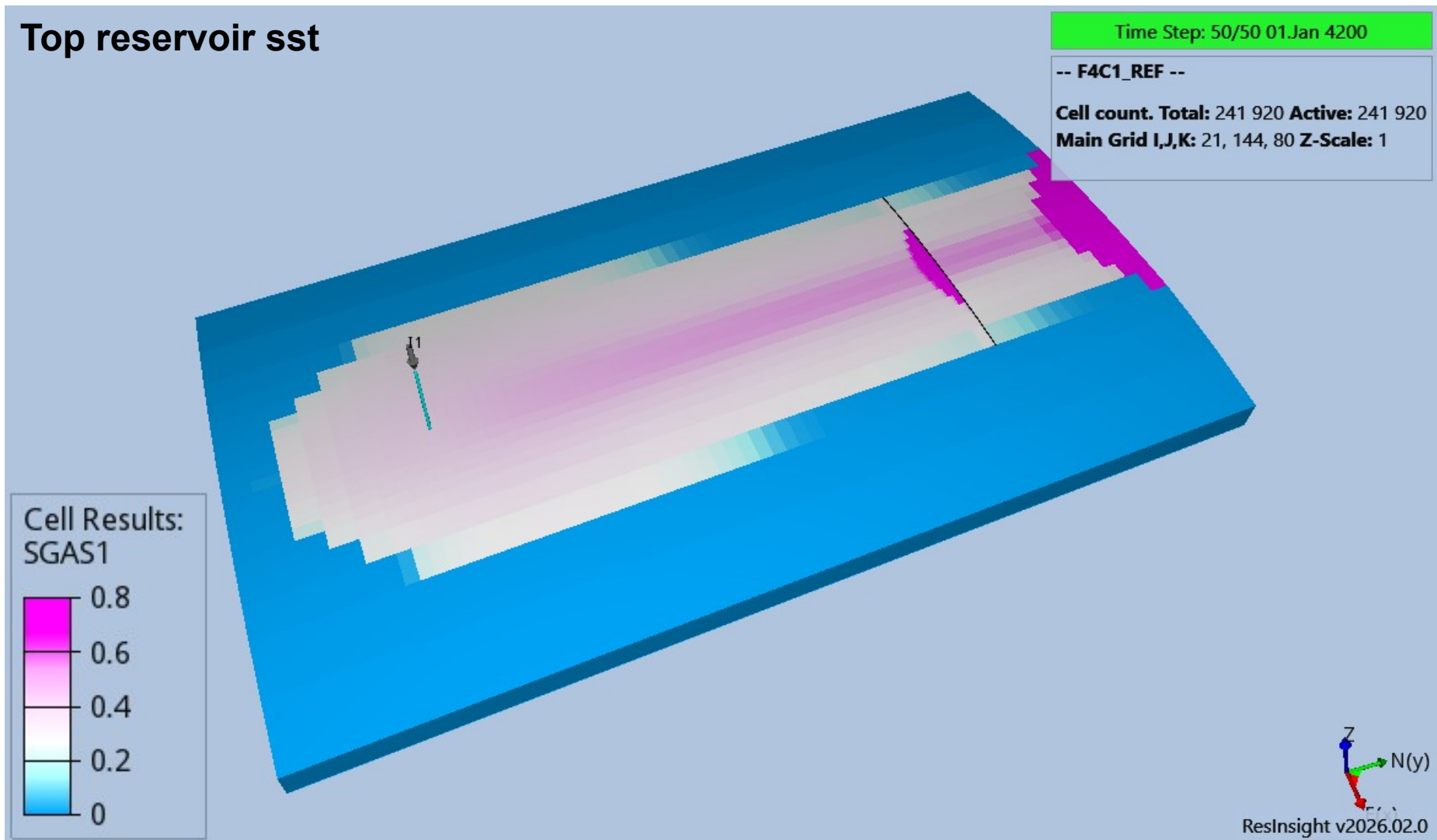
DB

matrix

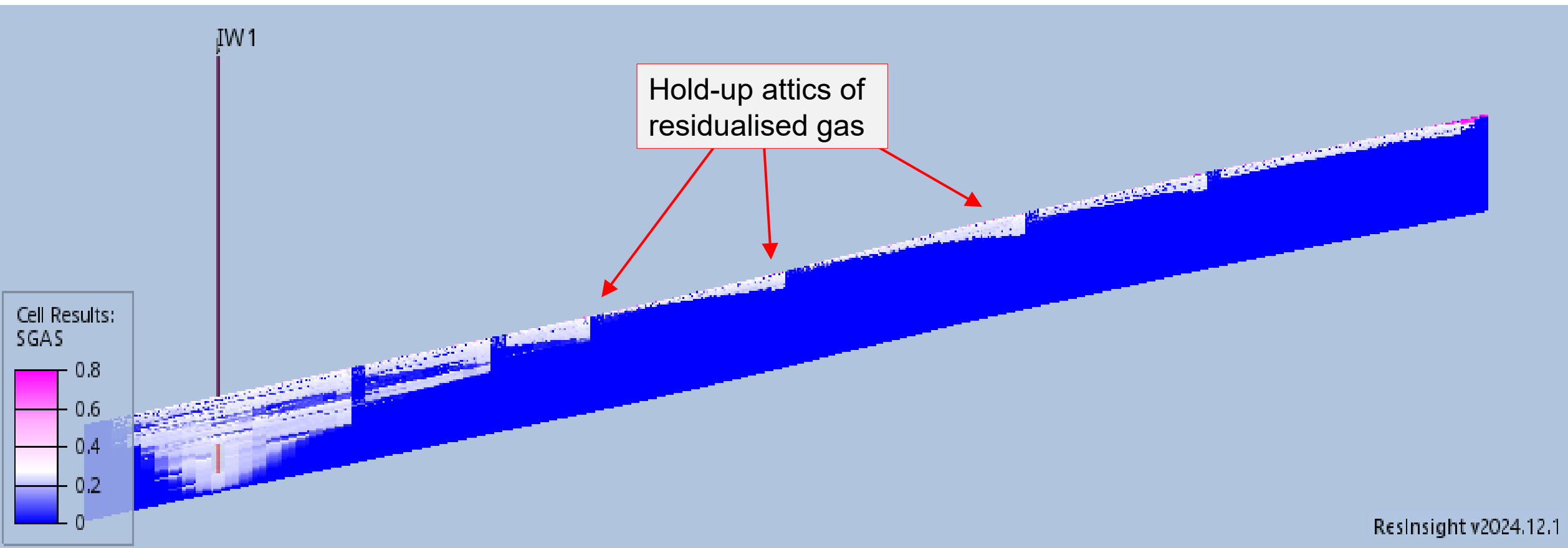
5mm increments



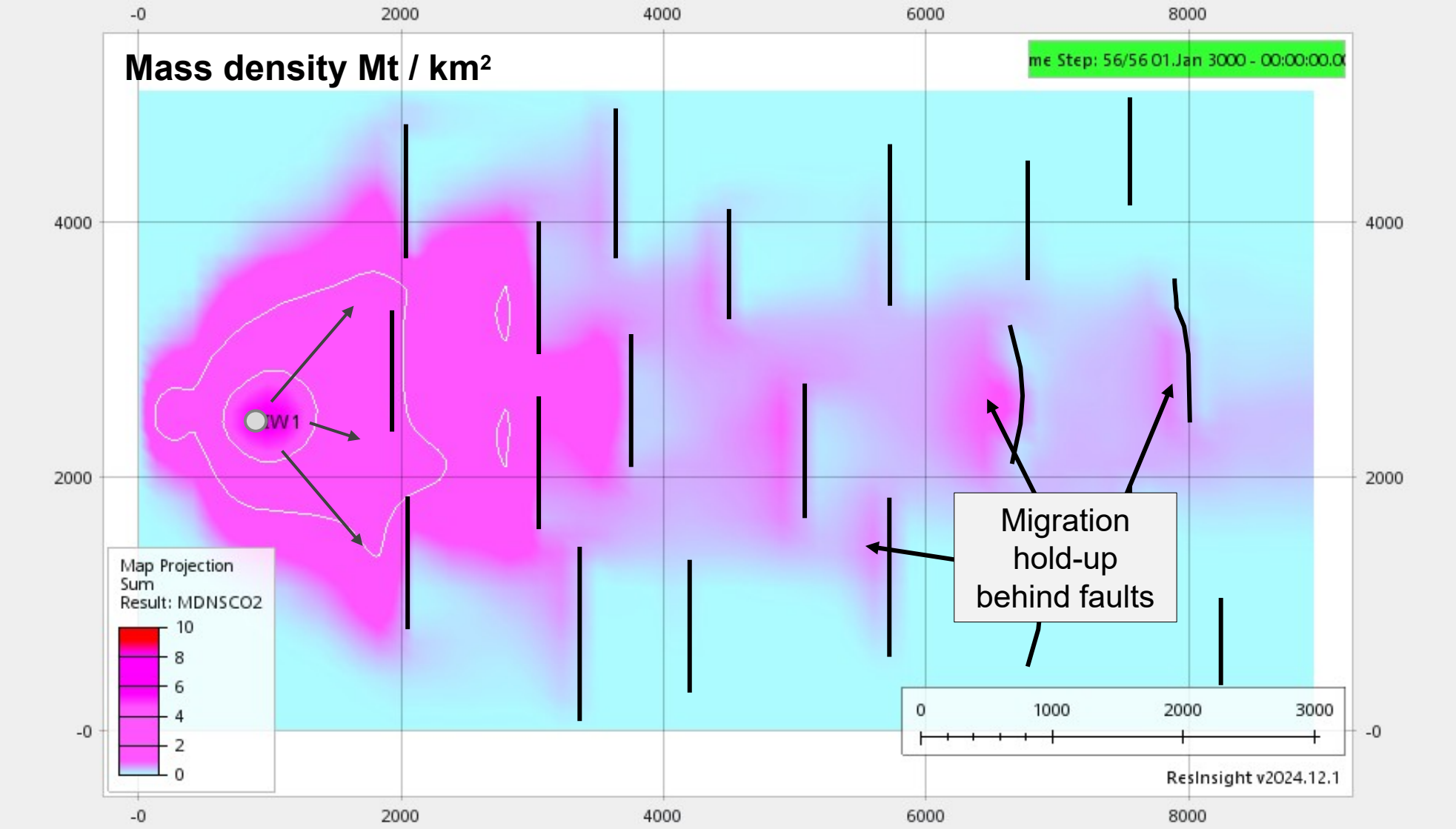
3D plume model



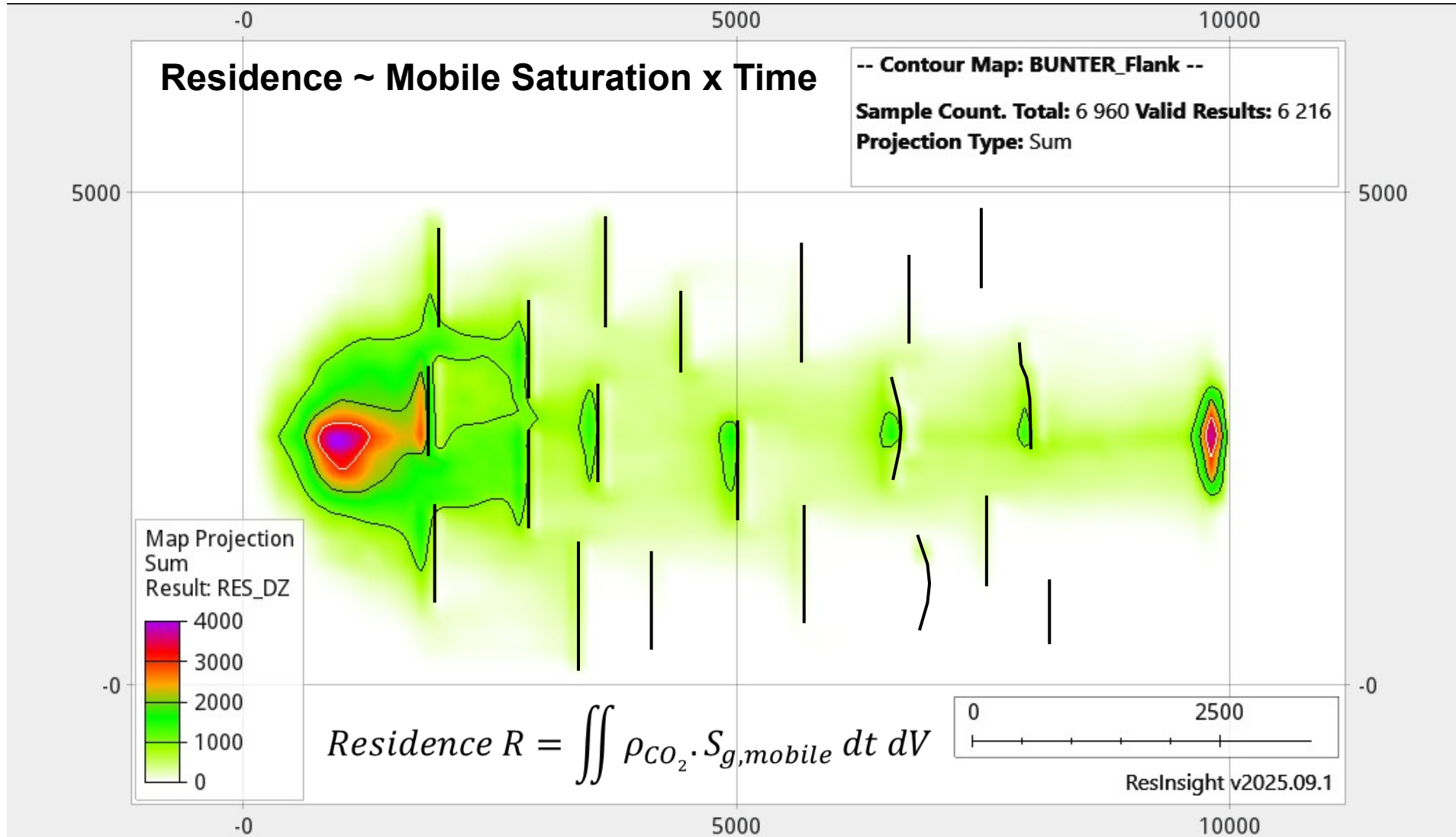
The 'salmon ladder'



Mass density of plume



Cumulative residence mapping



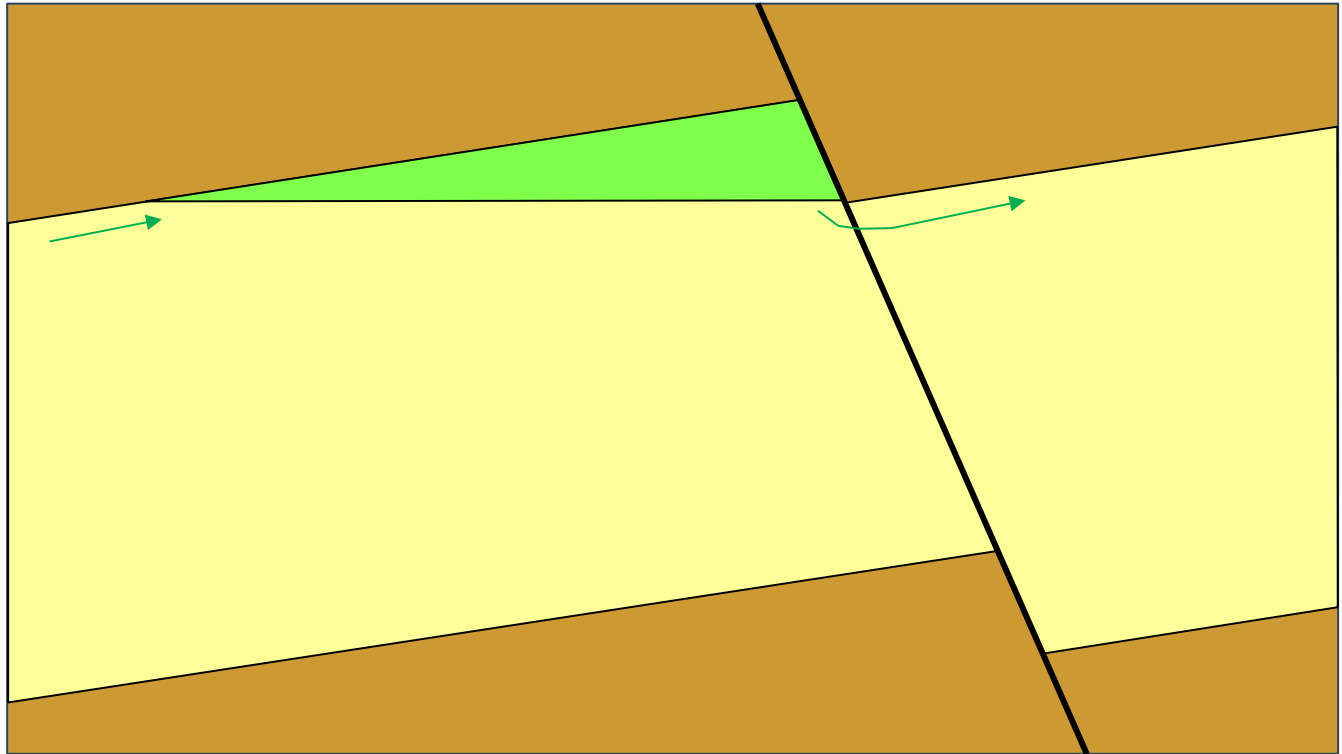
Total residence
~ 2000 Mt.yrs

Structural trapping effect

Fault displacement offsets
porous reservoir sands

CO₂ trapped in 'wedge'

May soak upwards into
overburden

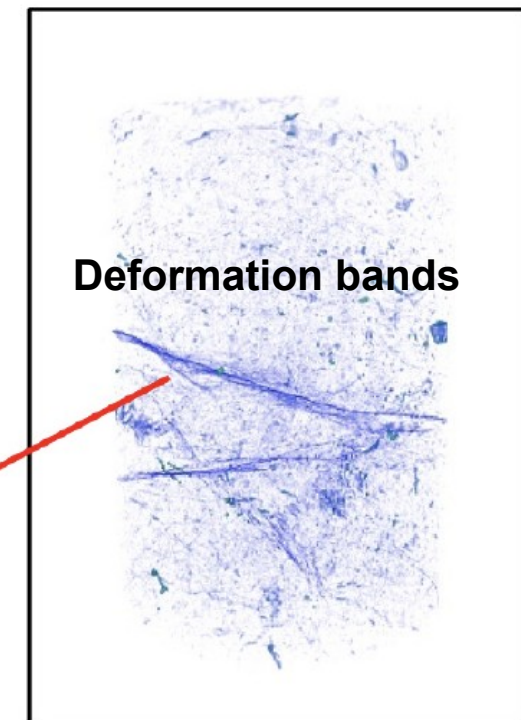
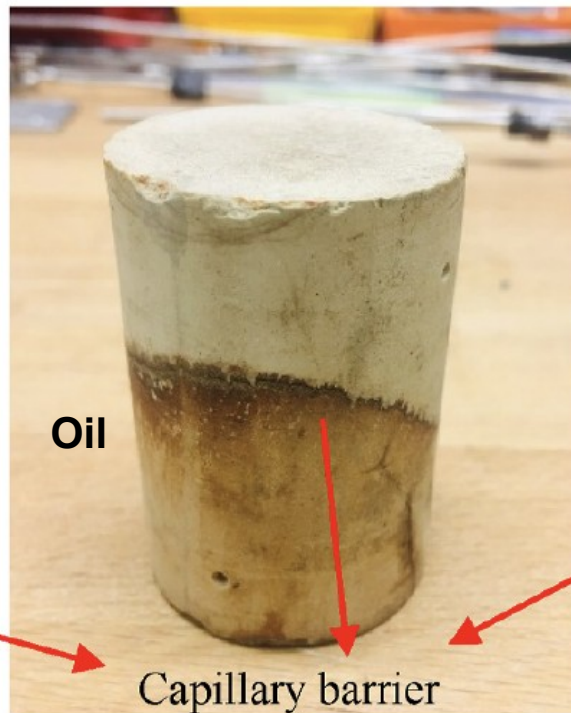


Capillary trapping effect

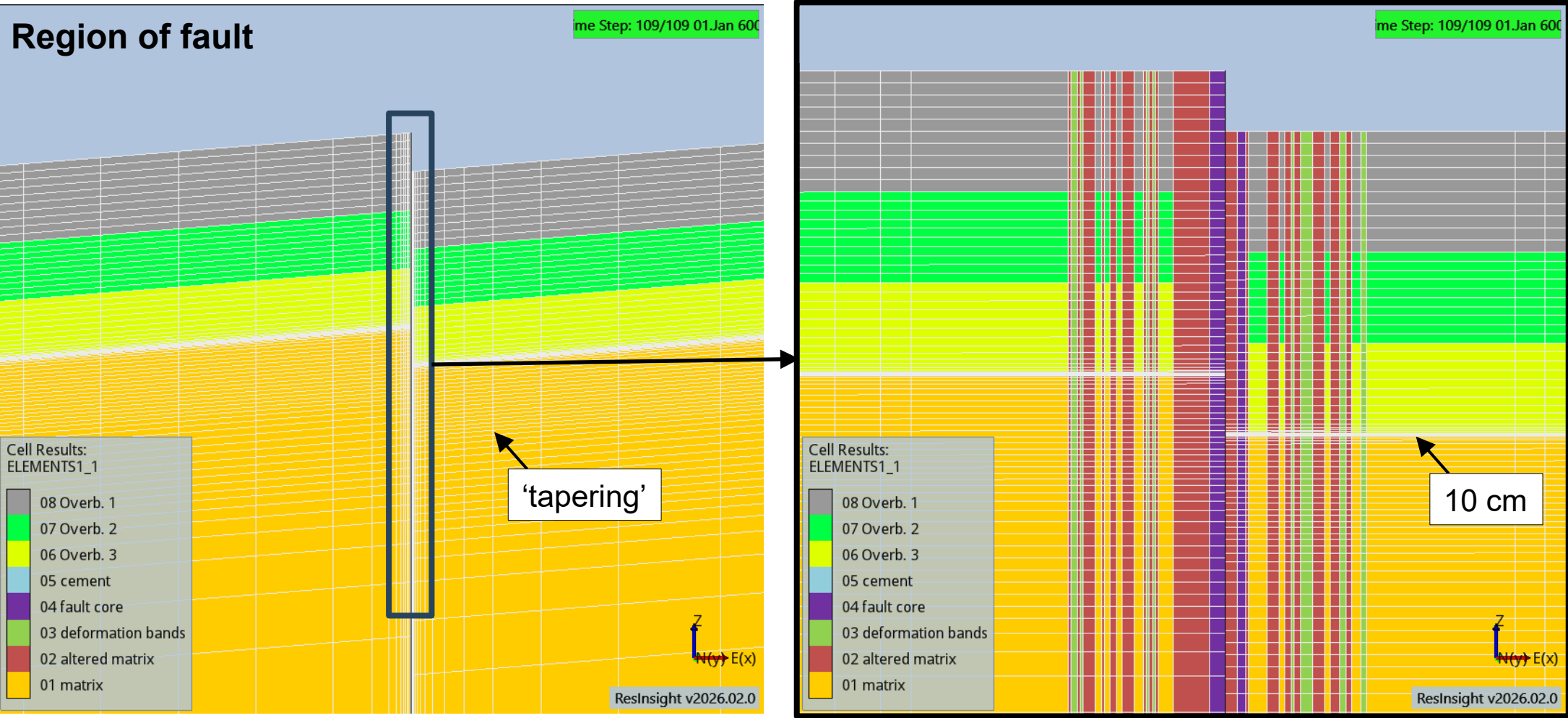
Fault elements (deformation bands, fault core) ... lower permeability and/or altered pore structure

Increased capillary entry pressure $P_{ce} \sim \sqrt{\phi/k}$

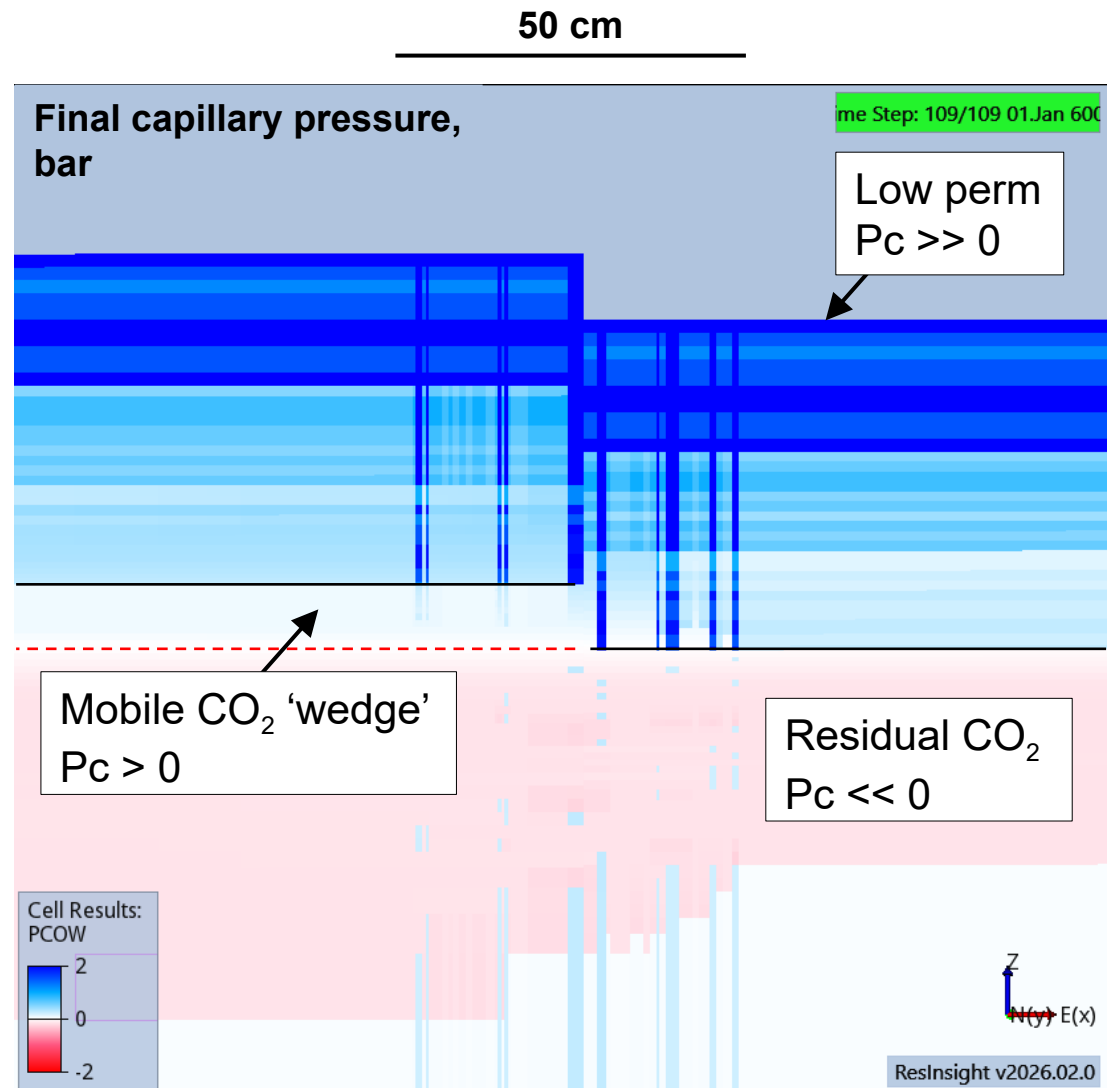
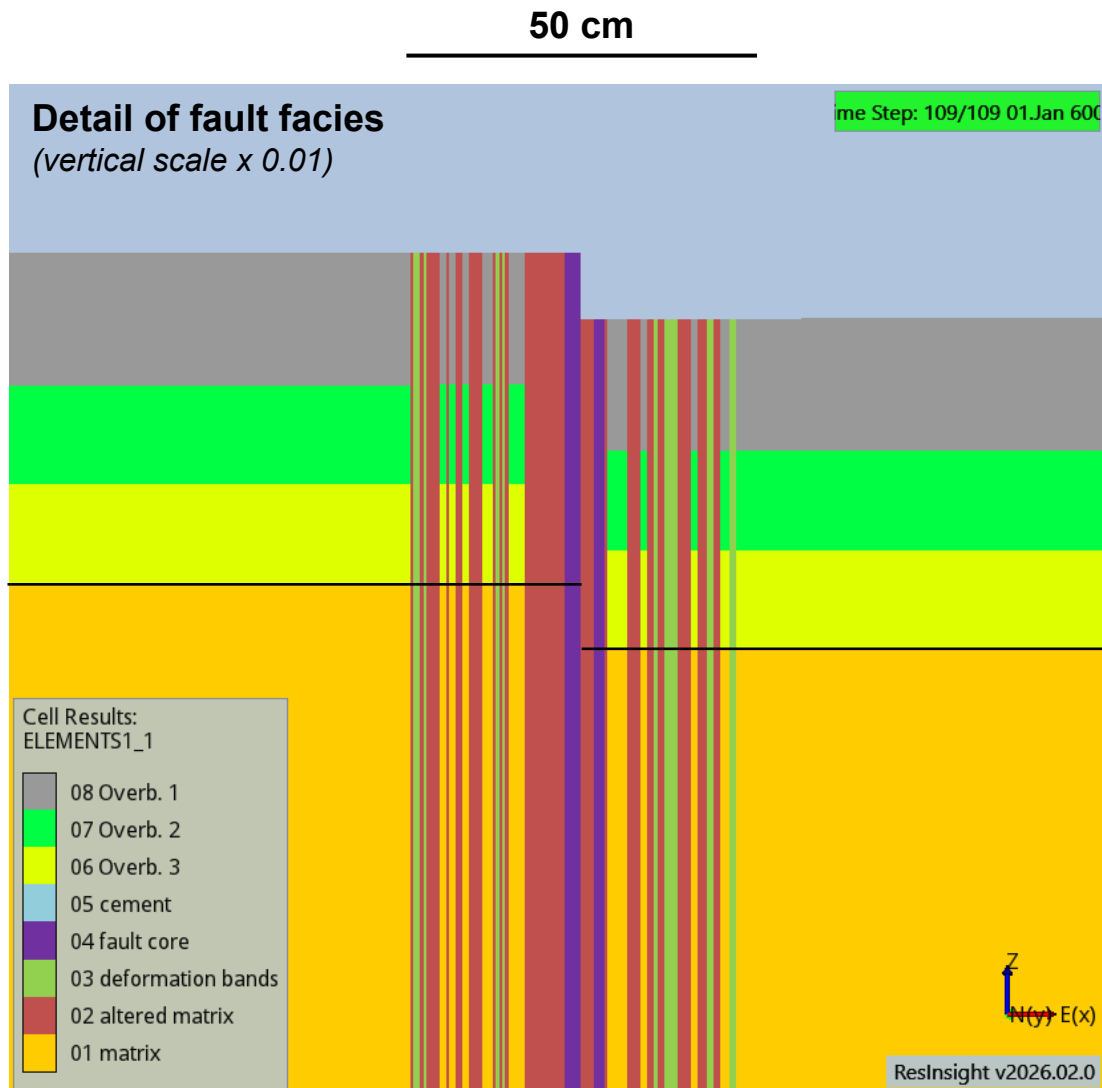
Holds back column of non-wetting fluid such as CO_2 (below core plug with oil)



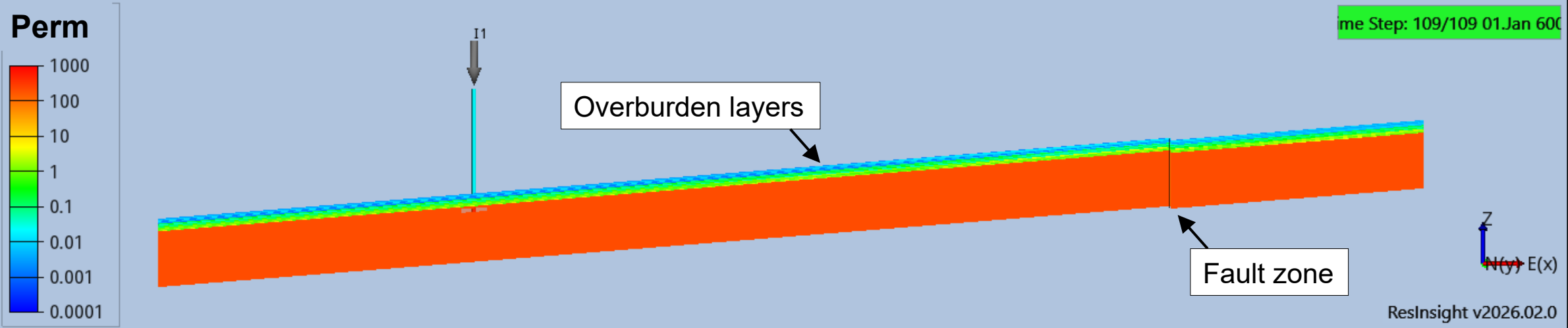
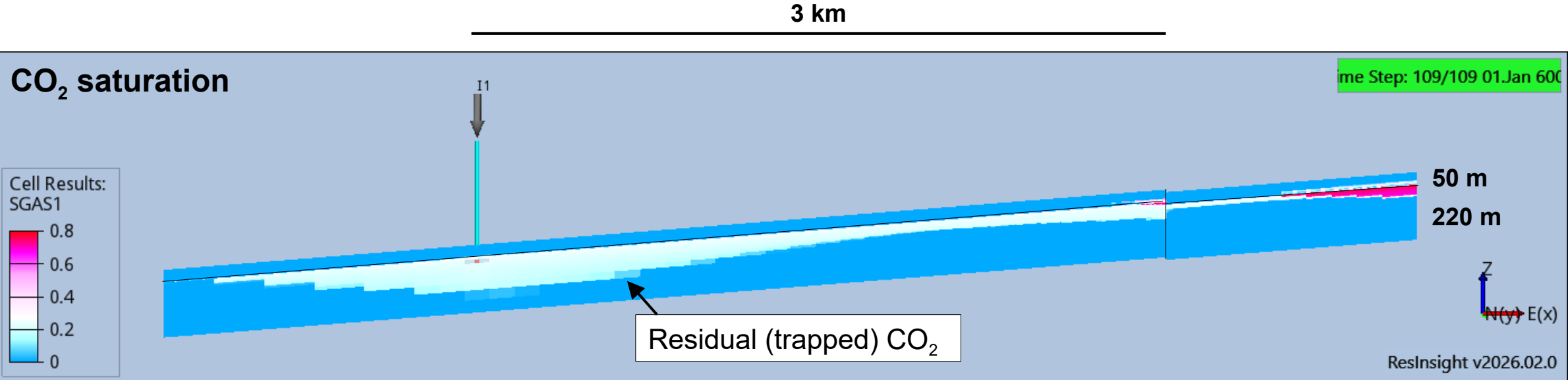
Grid choice



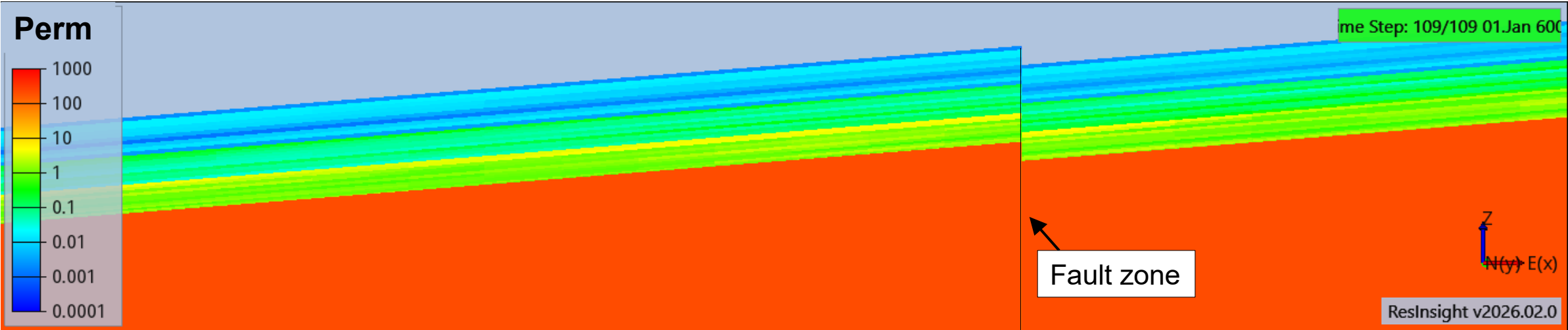
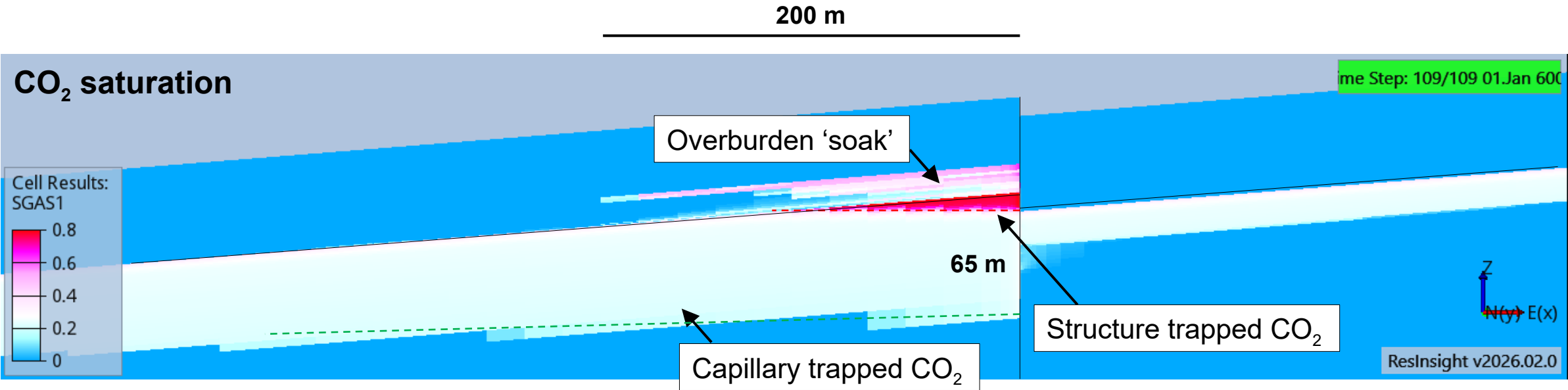
Capillary pressure within fault zone



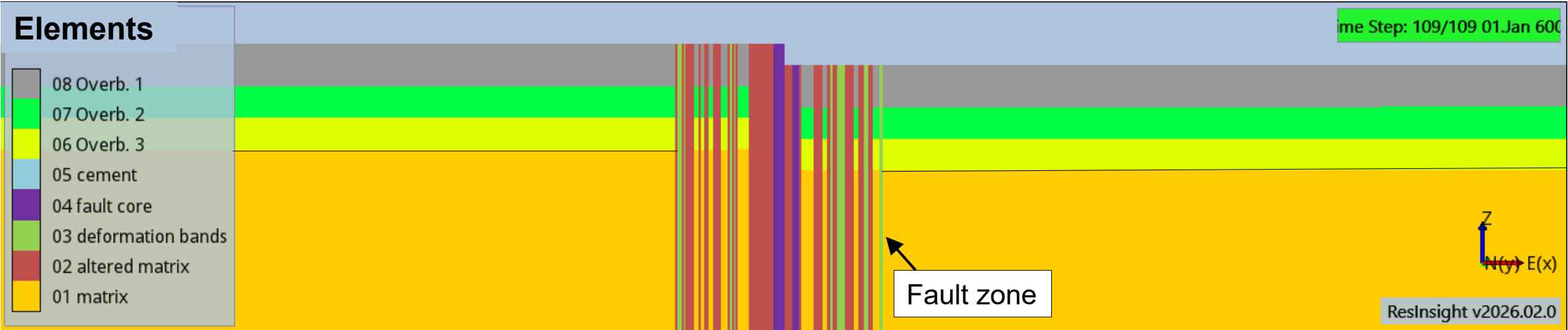
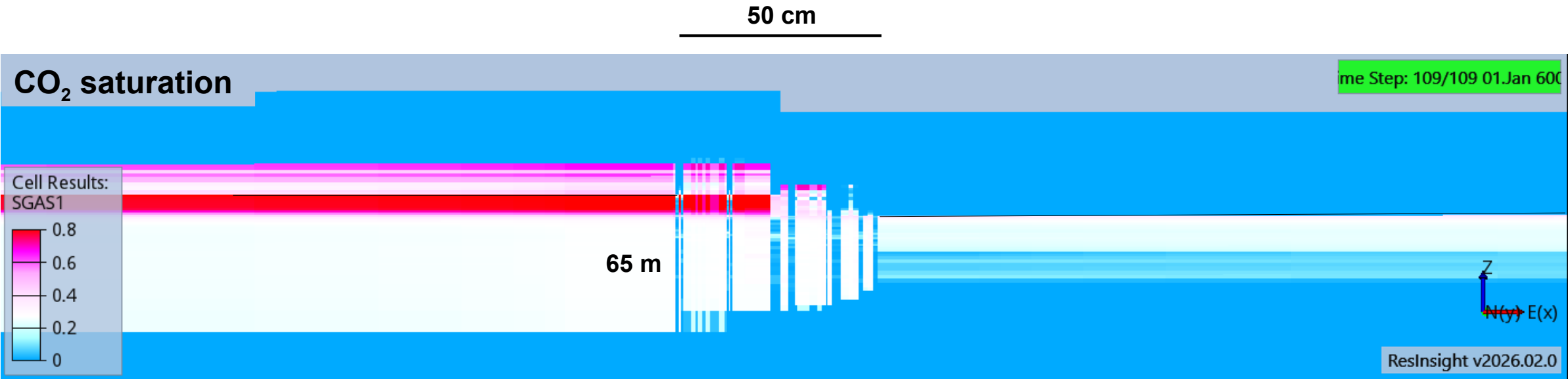
Plume cross section (1) – overview



Plume cross section (2) – close up

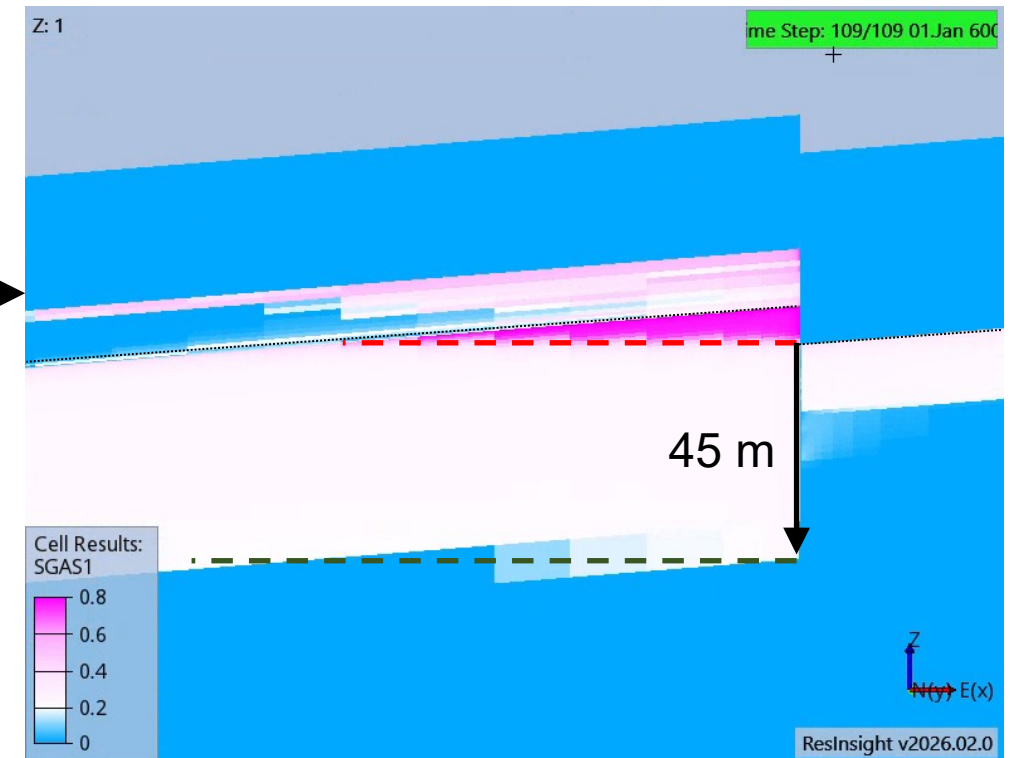
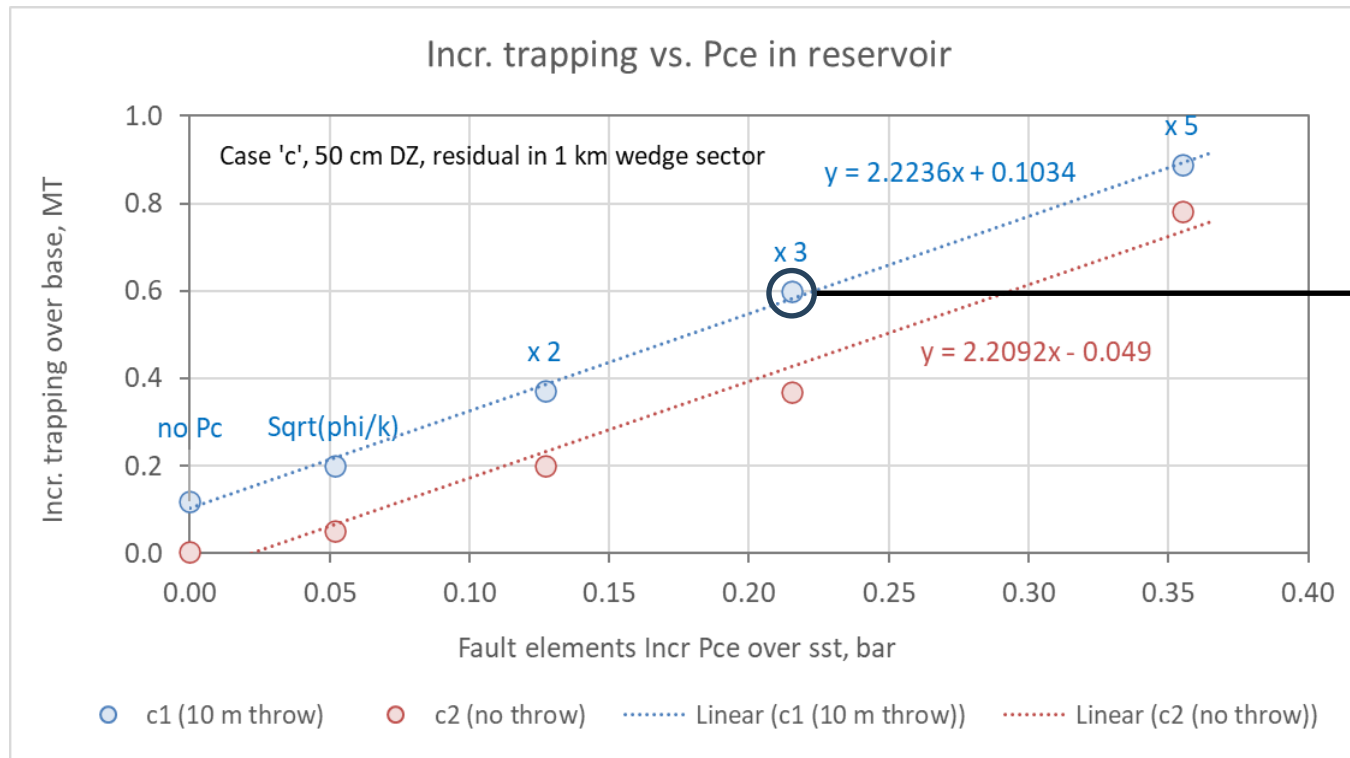


Plume cross section (3) – extreme close up



Static and dynamic trapping at fault

Trapping in reservoir – static (structure) + dynamic (capillary entry pressure)

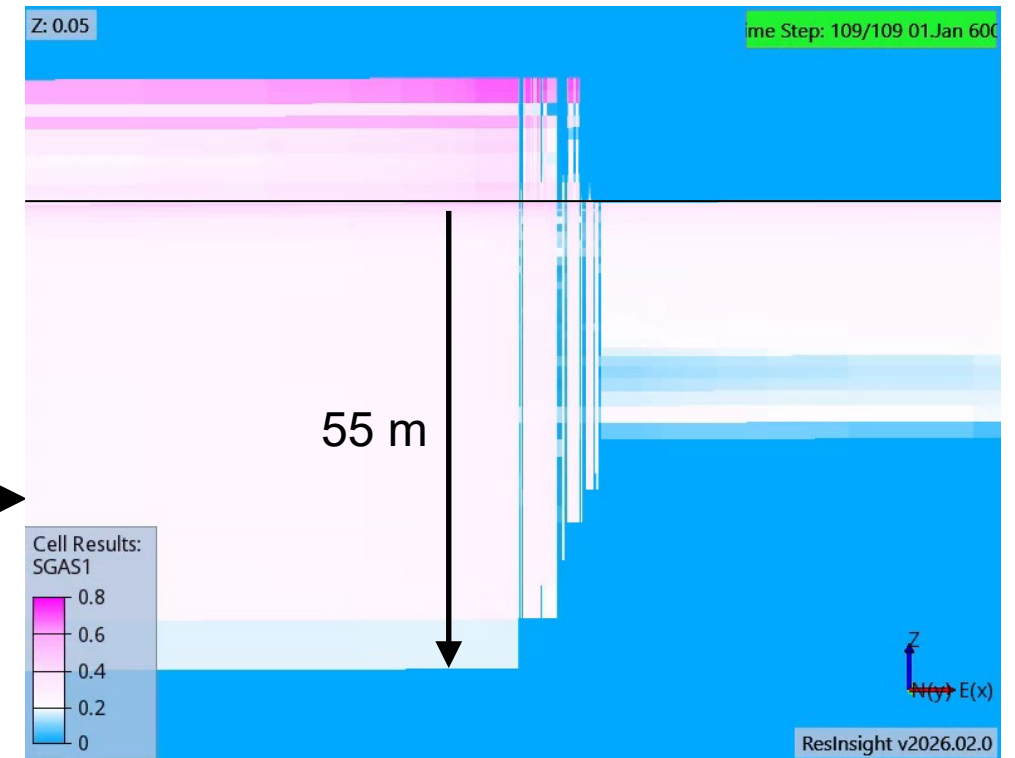
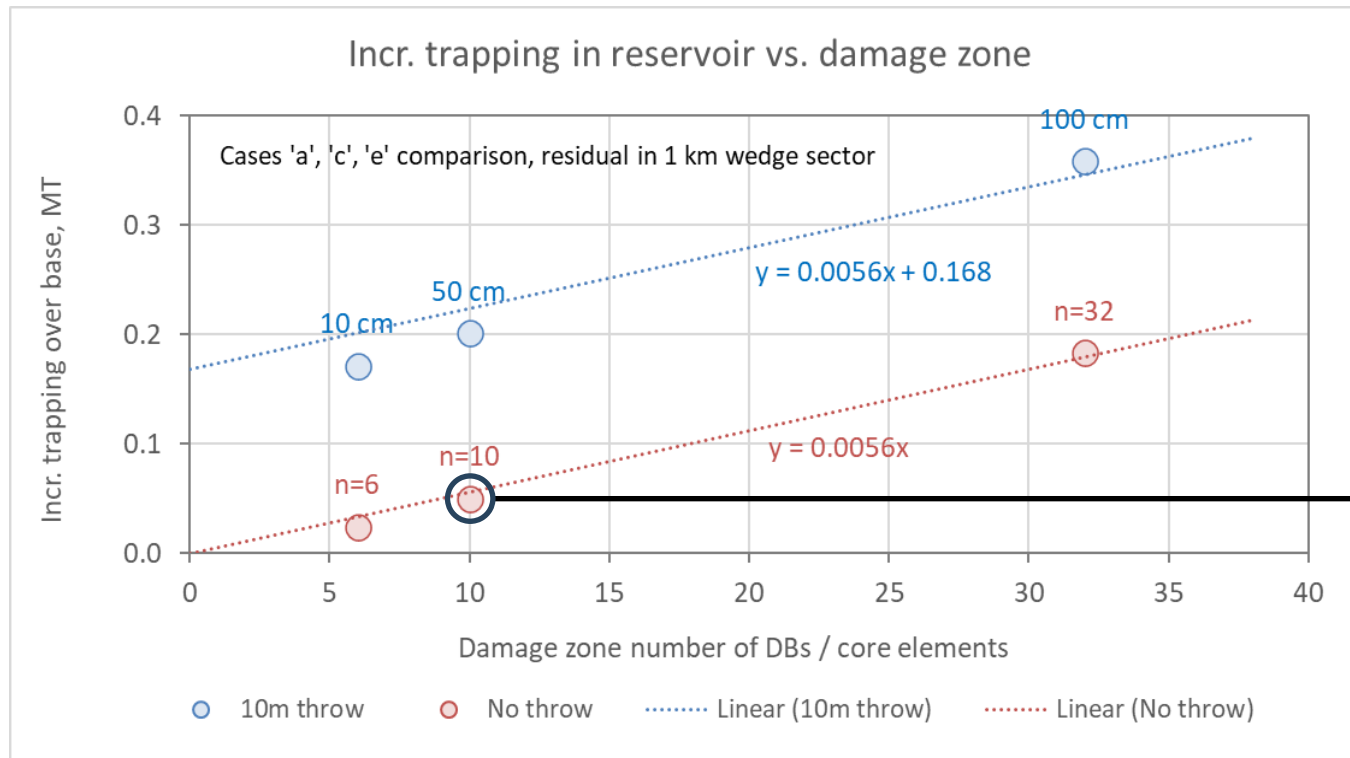


Static trapping (structure) ~ 0.1 Mt for a 10 m wedge

Dynamic trapping (entry pressure) ~ 0.1 Mt per 50 mbar entry pressure

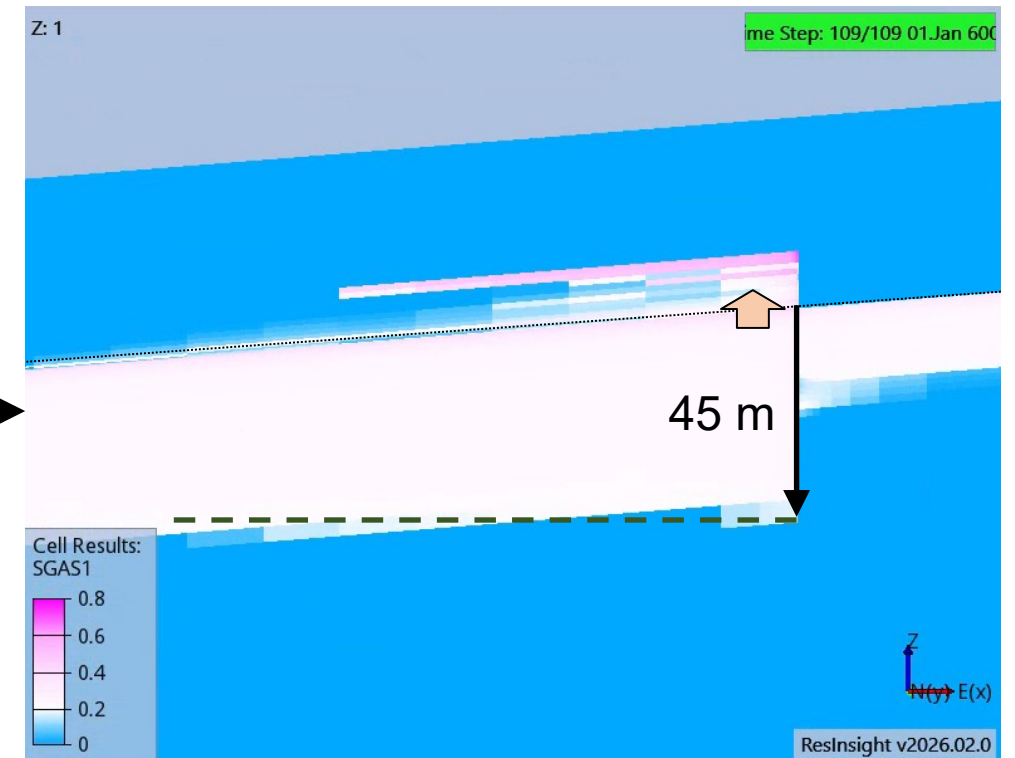
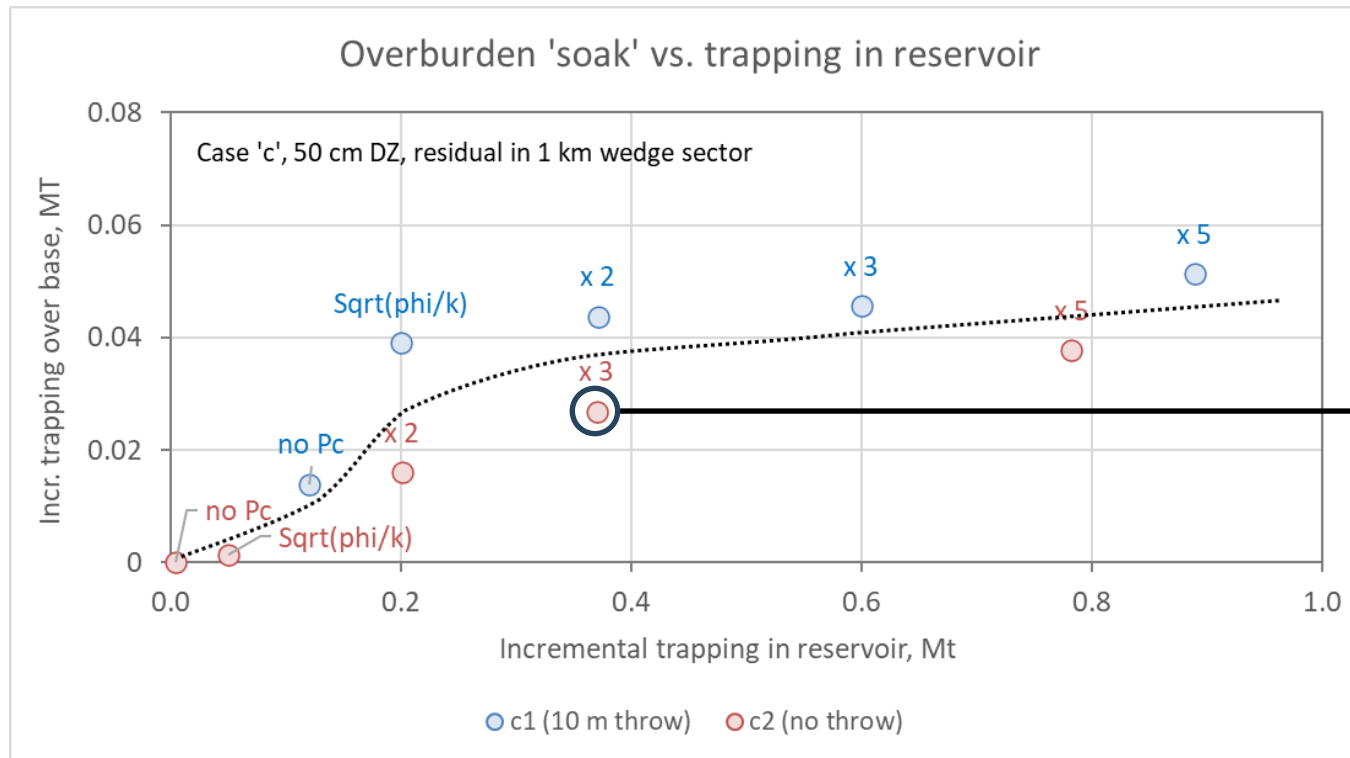
Effect of damage zone width / complexity

Trapping in reservoir scales with number of baffling fault elements (DBs, fault core)



Overburden 'soak'

Trapping in overburden ... lower but trending upwards with volume trapped in reservoir



Overburden soak ~ available mobile gas x time

Migration Assisted Storage

CO₂ area mass density

- Mt per km²

Injector area

- +/- 1.5 km around well
- Storage ~ 10 Mt

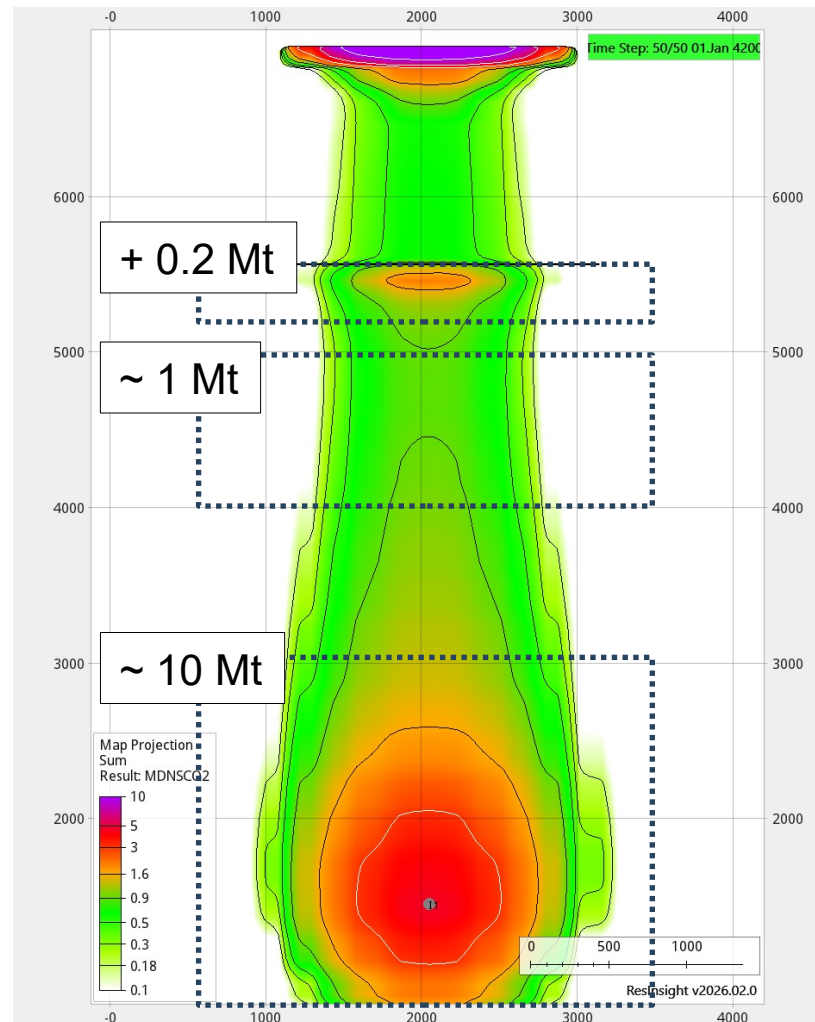
Plume

- Av. width ~ 1 km
- Storage ~ 1 Mt / km

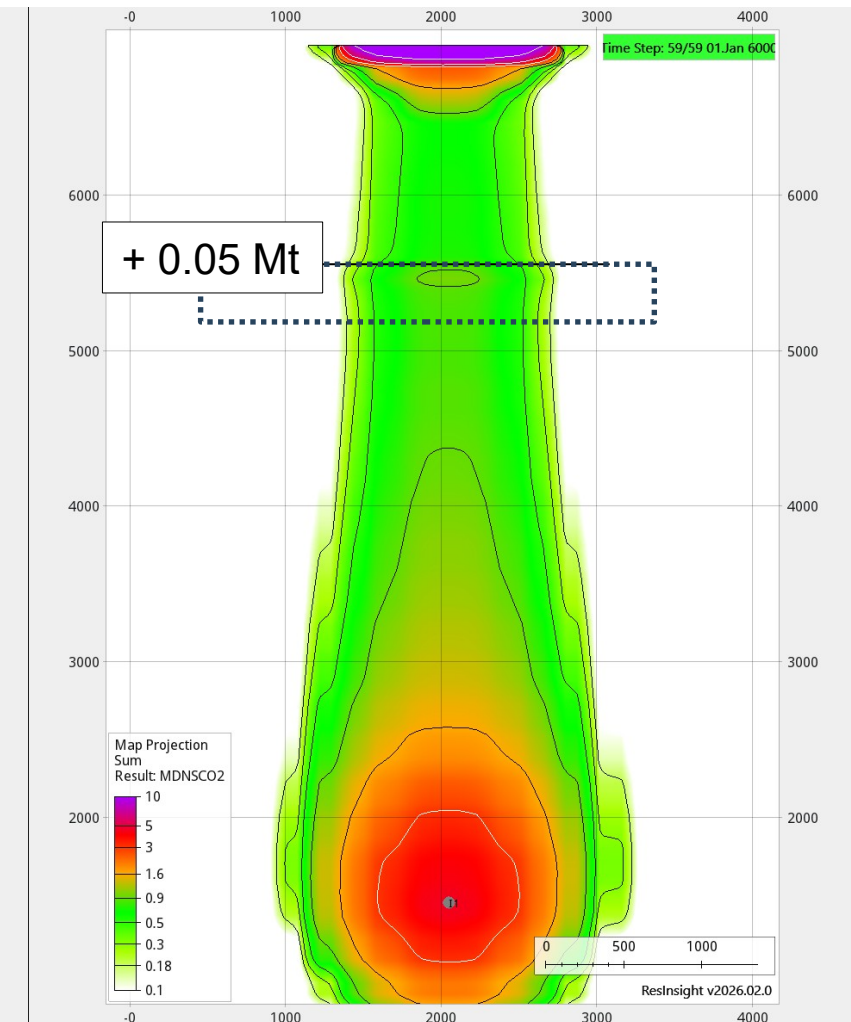
Faults

- Additional storage
- Model case ~ 0.1 Mt

Fault trapping, 10m throw, Mt/km²



No throw case, Mt/km²



Incremental trapping and *residence*

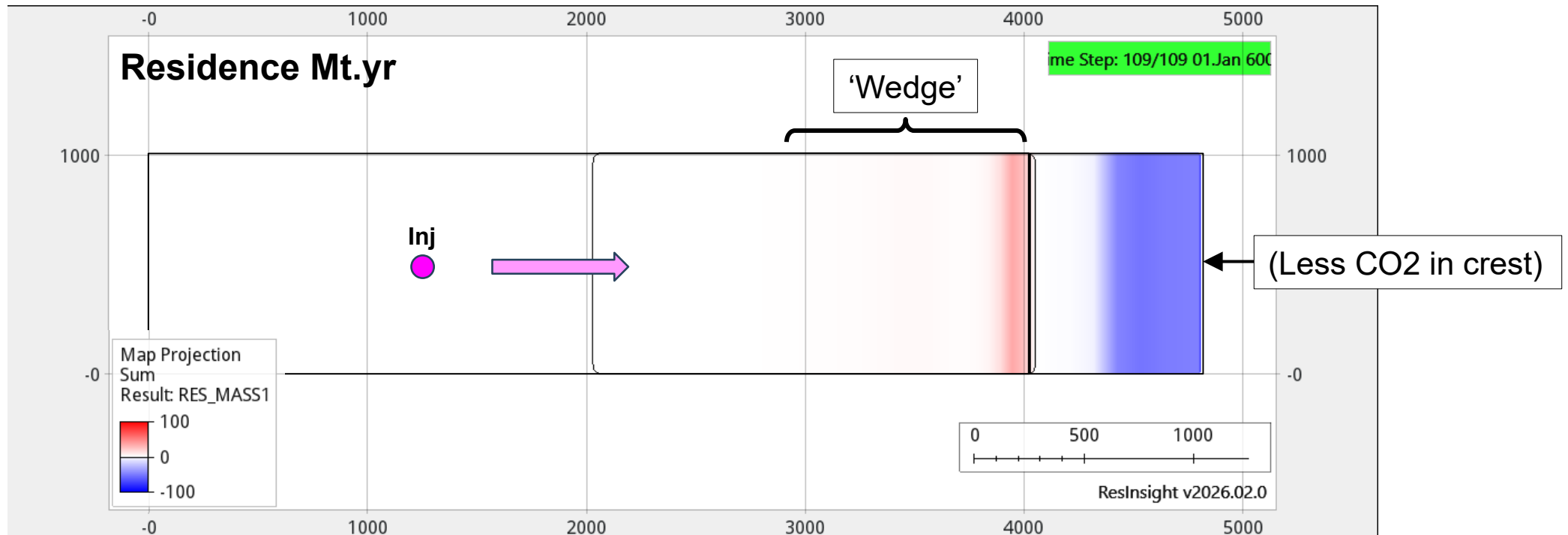
Example from 2D sector model, fault 10 m, structure dip 4°

Incremental over base case – plume with no fault

Mobile CO₂ trapped in ~ 1 km ‘wedge’

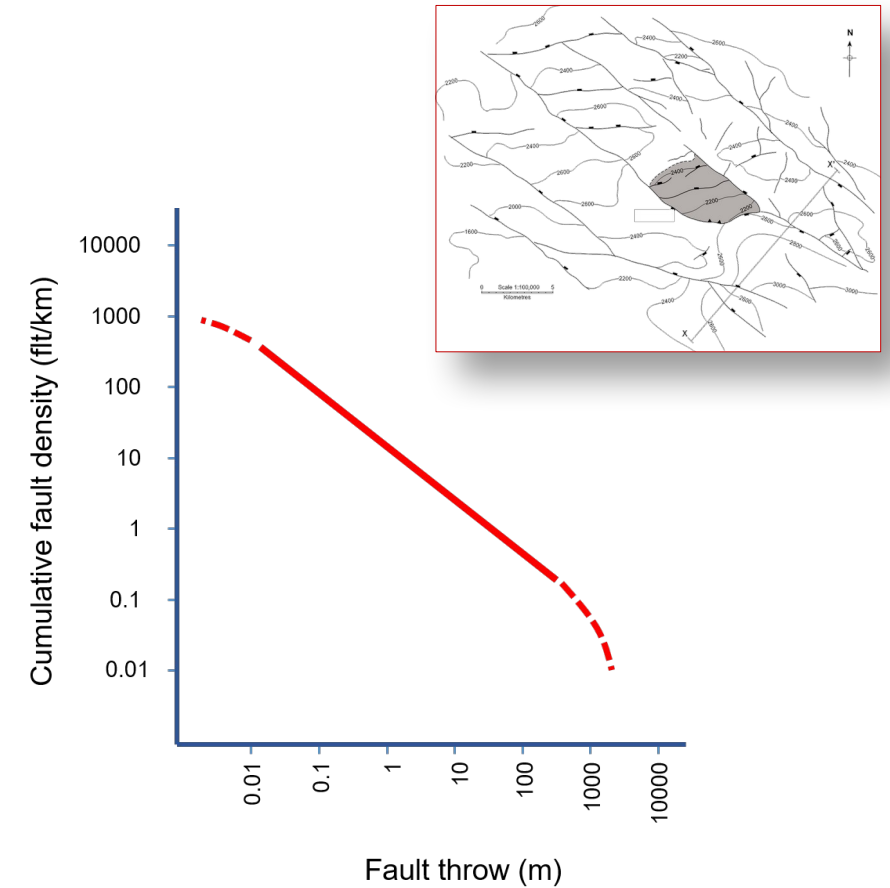
Incr. Trapping ~ 0.2 Mt
Residence ~ 200 Mt.yrs

$$\text{Residence } R = \iint \rho_{\text{CO}_2} \cdot S_{g,\text{mobile}} dt dV$$



... then a thought ...

*How many faults are there in a
100km long aquifer ... ?*



See also Nicol, Walsh, Watterson & Gillespie, 1996

Scale-up to a regional fault system

Model calibration

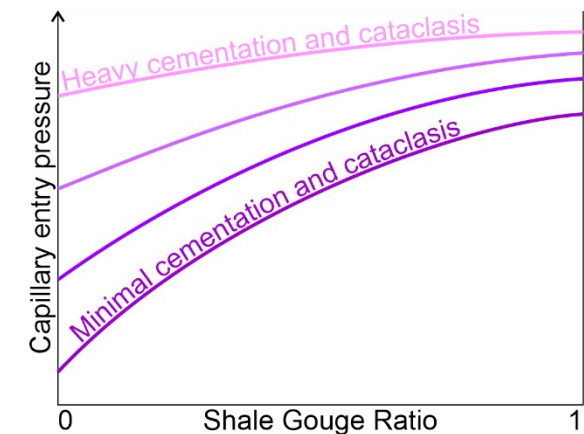
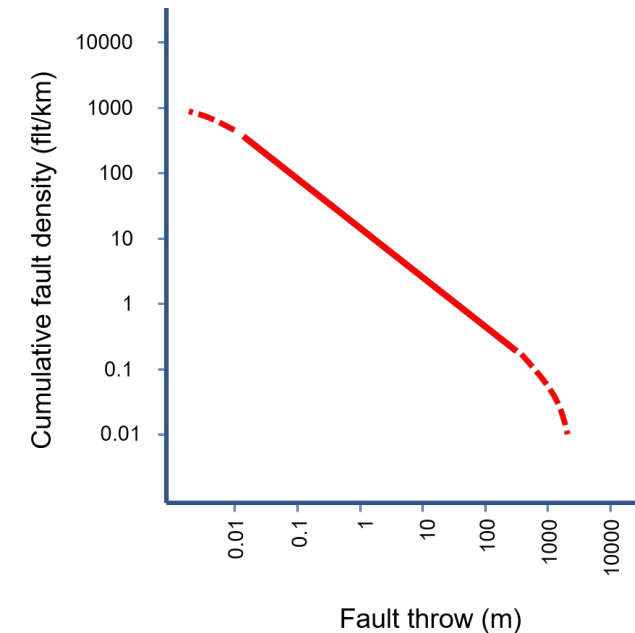
- 'Magnitude' 10 m fault $\rightarrow$ ~ 0.1 Mt structural effect, ~ 0.1 Mt capillary effect
- Incremental storage scaled to flank faults with range of sizes

Fault properties vs. magnitude

- Fault frequency / spacing ... power law exponent
- Fault DBs / core permeability ... no evidence for perm scaling
- Deformation bands ... harden and become more numerous with deformation

Potential for incremental storage on flank

- Integrate 20m (seismic scale) down to ~ 10 cm (strain hardening)
- Structural effect ... 0.4 Mt ... referenced to 2 km spacing for 10 m fault
- Capillary effect ... 0.4 Mt ... $P_{ce} \sim \sqrt{\phi/k}$, no chemical enhancement
- Overburden soak ... adds further 10-20%

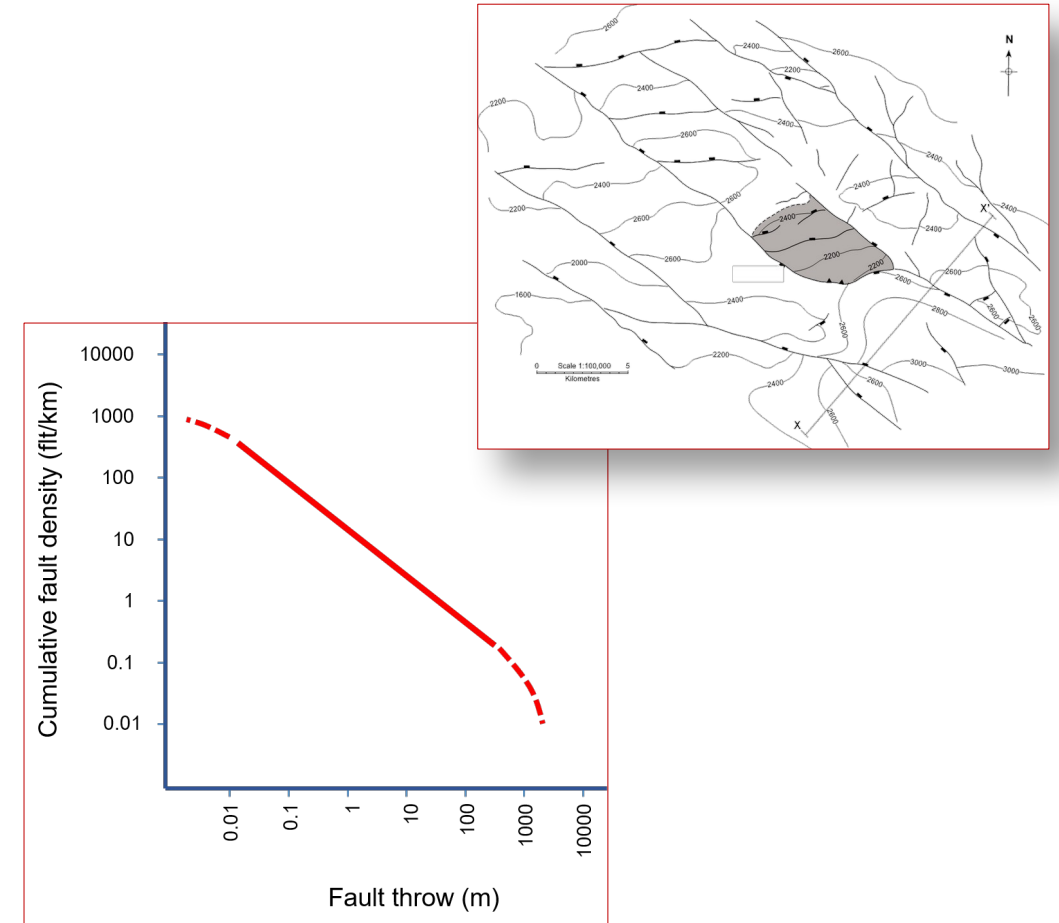


So

Scaling up

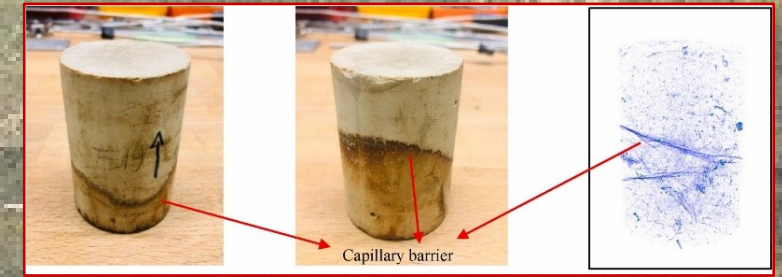
Impact of cumulative
residence *(for these cases)*

$\sim 1 \text{ Mt} / \text{km}$



Workflows for the CCS projects

Still dealing with heterogeneity,
.... but with different
sensitivities and different tools



Fine-scale structural model elements
required

Fault rock property scenarios *needed* to
quantify impact

Workflows involve very high resolution
models, then scale-up using structural rules

Current (simpler) coarse models are missing
some good storage news

